

# Highly Integrated Wireless Receiver Qi (WPC v1.1) Compliant Power Supply

Check for Samples: bq51003

### **FEATURES**

- Integrated Wireless Power Supply Receiver Solution - Optimized for 2.5-W Applications
  - 93% Overall Peak AC-DC Efficiency
  - Full Synchronous Rectifier
  - WPC v1.1 Compliant Communication Control
  - Output Voltage Conditioning
  - Only IC Required Between Rx coil and Output
- Wireless Power Consortium (WPC) v1.1
   Compliant (FOD Enabled) Highly Accurate
   Current Sense
- Dynamic Rectifier Control for Improved Load Transient Response
- Dynamic Efficiency Scaling for Optimized Performance Over wide Range of Output Power
- Adaptive Communication Limit for Robust Communication
- Supports 20-V Maximum Input
- Low-power Dissipative Rectifier Overvoltage Clamp (V<sub>RECT-OVP</sub> = 15 V)
- Thermal Shutdown
- Multifunction NTC and Control Pin for Temperature Monitoring, Charge Complete and Fault Host Control
- 1.9-mm x 3.0-mm DSBGA

#### **APPLICATIONS**

- WPC Compliant Receivers
- Cell Phones, Smart Phones
- Headsets
- Digital Cameras
- Portable Media Players
- Hand-held Devices

### DESCRIPTION

The bq51003 is an advanced, integrated, receiver IC for wireless power transfer in portable applications. The device provides the AC/DC power conversion while integrating the digital control required to comply with the Qi v1.1 communication protocol. Together with the bq500210 transmitter controller, the bq51003 enables a complete contact-less power transfer system for a wireless power supply solution. By using near-field inductive power transfer, the receiver coil embedded in the portable device receives the power transmitted by the transmitter coil via mutually coupled inductors. The AC signal from the receiver coil is then rectified and regulated to be used as a power supply for down-system electronics. Global feedback is established from the secondary to the transmitter in order to stabilize the power transfer process via back-scatter modulation. This feedback is established by using the Qi v1.1 communication protocol supporting up to 2.5-W applications.

The device integrates a low-impedance full synchronous rectifier, low-dropout regulator, digital control, and accurate voltage and current loops.

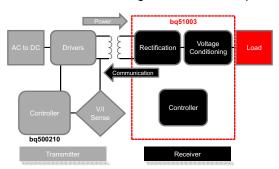


Figure 1. Wireless Power Consortium (WPC or Qi) Inductive Power System



#### ORDERING INFORMATION

PART NUMBER	NUMBER MARKING FUNCTION		PACKAGE	ORDERING NUMBER (Tape and Reel)	QUANTITY
haE1002	haE1002	FV Degulated Davier Cumply	DCDCA VED	bq51003YFPR	3000
bq51003	bq51003	5V Regulated Power Supply	DSBGA-YFP	bq51003YFPT	250

#### **AVAILABLE OPTIONS**

DEVICE	FUNCTION	WPC VERSION	V <sub>RECT-OVP</sub>	V <sub>OUT-(REG)</sub>	OVER CURRENT SHUTDOWN	AD-OVP	TERMINATION	COMMUNICATION CURRENT LIMIT <sup>(1)(2)</sup>
bq51003	5-V Power Supply	v1.1	15 V	5 V	Disabled	Disabled	Disabled	Adaptive + 1 s Hold-Off

<sup>(1)</sup> Enabled if EN2 is low and disabled if EN2 is high

### **ABSOLUTE MAXIMUM RATINGS**(1)(2)

over operating free-air temperature range (unless otherwise noted)

		VAL	LINUTO	
		MIN	UNITS	
	AC1, AC2	-0.8	20	V
	RECT, COMM1, COMM2, OUT, CHG, CLAMP1, CLAMP2	-0.3	20	V
Input voltage	AD, AD-EN	-0.3	30	V
	BOOT1, BOOT2	-0.3	26	V
	EN1, EN2, FOD, TS-CTRL, ILIM	-0.3	7	V
Input current	AC1, AC2		1	A(RMS)
Output current	OUT		525	mA
Outrot sink sument	CHG		15	mA
Output sink current	COMM1, COMM2		1	Α
Junction temperature, T <sub>J</sub>		-40	150	°C
Storage temperature, T <sub>STG</sub>		-65	150	°C
FCD Dation (400 of 4.5 kg)	Human Body Model (HBM)	2		kV
ESD Rating (100 pF, 1.5 k $\Omega$ )	Charge Device Model (CDM)	500		V

<sup>(1)</sup> All voltages are with respect to the VSS terminal, unless otherwise noted.

#### THERMAL INFORMATION

	TUEDMAL METDIC(1)	YFP	LINUTO
	THERMAL METRIC <sup>(1)</sup>	28 PINS	UNITS
$\theta_{JA}$	Junction-to-ambient thermal resistance	58.9	
$\theta_{\text{JCtop}}$	Junction-to-case (top) thermal resistance	0.2	
$\theta_{JB}$	Junction-to-board thermal resistance	9.1	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	1.4	*C/VV
ΨЈВ	Junction-to-board characterization parameter	8.9	
$\theta_{JCbot}$	Junction-to-case (bottom) thermal resistance	n/a	

(1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

Submit Documentation Feedback

<sup>(2)</sup> Communication current limit is disabled for 1 second at startup

<sup>(2)</sup> Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT
$V_{IN}$	Input voltage range	RECT	4		10	V
I <sub>IN</sub>	Input Current	RECT			500	mA
I <sub>OUT</sub>	Output Current	OUT			500	mA
I <sub>AD-EN</sub>	Sink Current	AD-EN			1	mA
I <sub>COMM</sub>	COMM Sink Current	COMM			500	mA
TJ	Junction Temperature		0		125	°C

### **TYPICAL APPLICATION SCHEMATICS**

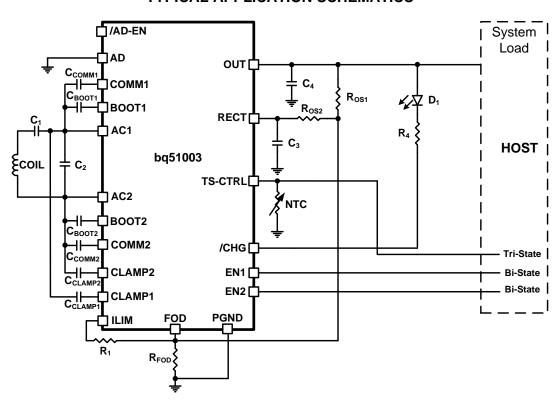


Figure 2. bq51003 Used as a Wireless Power Receiver and Power Supply for System Loads Only One of  $R_{\rm OS1}$  or  $R_{\rm OS2}$  Needed



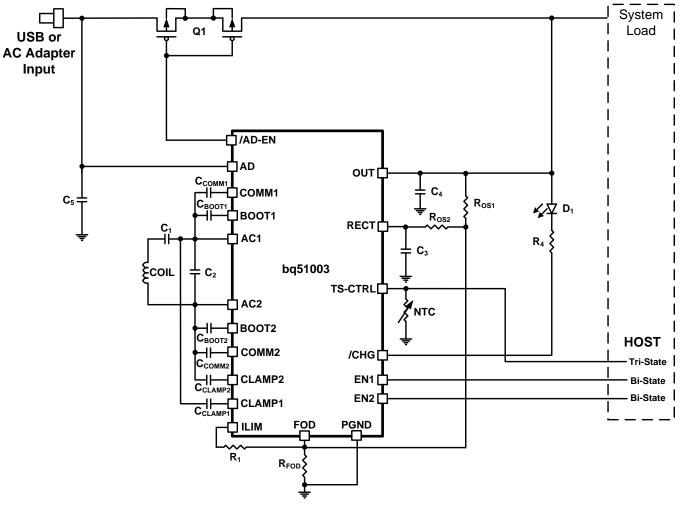


Figure 3. bq51003 Used as a Wireless Power Receiver and Power Supply for System Loads with Adapter Power-Path Multiplexing Only One of  $R_{\rm OS1}$  or  $R_{\rm OS2}$  Needed



# **ELECTRICAL CHARACTERISTICS**

over operating free-air temperature range, 0°C to 125°C (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
UVLO	Undervoltage lock-out	$V_{RECT}$ : 0 V $\rightarrow$ 3 V	2.6	2.7	2.8	V
\/	Hysteresis on UVLO	V <sub>RECT</sub> : 3 V → 2 V		250		mV
V <sub>HYS</sub>	Hysteresis on OVP	V <sub>RECT</sub> : 16 V → 5 V		150		mV
V <sub>RECT-OVP</sub>	Input overvoltage threshold	V <sub>RECT</sub> : 5 V → 16 V	14.5	15	15.5	V
	Dynamic V <sub>RECT</sub> threshold 1	I <sub>LOAD</sub> < 0.1 x I <sub>IMAX</sub> (I <sub>LOAD</sub> rising)		7.08		
	Dynamic V <sub>RECT</sub> threshold 2	$0.1 \times I_{IMAX} < I_{LOAD} < 0.2 \times I_{IMAX}$ ( $I_{LOAD}$ rising)		6.28		V
V <sub>RECT-REG</sub>	Dynamic V <sub>RECT</sub> threshold 3	$0.2 \times I_{IMAX} < I_{LOAD} < 0.4 \times I_{IMAX}$ ( $I_{LOAD}$ rising)		5.53		V
	Dynamic V <sub>RECT</sub> threshold 4	$I_{LOAD} > 0.4 \text{ x } I_{IMAX} (I_{LOAD} \text{ rising})$		5.11		
	V <sub>RECT</sub> TRACKING	In current limit voltage above V <sub>OUT</sub>		V <sub>O</sub> +0.25		
I <sub>LOAD</sub>	$\rm I_{LOAD}$ hysteresis for dynamic $\rm V_{RECT}$ thresholds as a % of $\rm I_{ILIM}$	I <sub>LOAD</sub> falling		4%		
V <sub>RECT-DPM</sub>	Rectifier undervoltage protection, restricts I <sub>OUT</sub> at V <sub>RECT-DPM</sub>		3	3.1	3.2	V
V <sub>RECT-REV</sub>	Rectifier reverse voltage protection at the output	$V_{RECT-REV} = V_{OUT} - V_{RECT},$ $V_{OUT} = 10 \text{ V}$		8	9	V
QUIESCENT	CURRENT					
	Active chip quiescent current consumption	$I_{LOAD} = 0 \text{ mA}, 0^{\circ}\text{C} \le T_{J} \le 85^{\circ}\text{C}$		8	10	mA
I <sub>RECT</sub>	from RECT	$I_{LOAD} = 300 \text{ mA},$ $0^{\circ}\text{C} \leq T_{J} \leq 85^{\circ}\text{C}$		2	3.0	mA
I <sub>OUT</sub>	Quiescent current at the output when wireless power is disabled (Standby)	V <sub>OUT</sub> = 5 V, 0°C ≤ T <sub>J</sub> ≤ 85°C		20	35	μΑ
I <sub>LIM</sub> SHORT	CIRCUIT					
R <sub>ILIM</sub>	Highest value of $I_{LIM}$ resistor considered a fault (short). Monitored for $I_{OUT} > 100 \text{ mA}$	$R_{ILIM}$ : 200 $\Omega \rightarrow$ 50 $\Omega$ . $I_{OUT}$ latches off, cycle power to reset			120	Ω
t <sub>DGL</sub>	Deglitch time transition from $\rm I_{LIM}$ short to $\rm I_{OUT}$ disable			1		ms
I <sub>LIM_SC</sub>	$\rm I_{LIM-SHORT,OK}$ enables the $\rm I_{LIM}$ short comparator when $\rm I_{OUT}$ is greater than this value	I <sub>LOAD</sub> : 0 mA → 200 mA	120	145	165	mA
	Hysteresis for I <sub>LIM-SHORT,OK</sub> comparator	$I_{LOAD}$ : 0 mA $\rightarrow$ 200 mA		30		mA
I <sub>OUT</sub>	Maximum output current limit, C <sub>L</sub>	Maximum I <sub>LOAD</sub> that will be delivered for 1 ms when I <sub>LIM</sub> is shorted			2.45	Α
OUTPUT						
V <sub>OUT-REG</sub>	Regulated output voltage	$I_{LOAD} = 500 \text{ mA}$	4.96	5.00	5.04	V
*OUT-REG	regulated output voltage	I <sub>LOAD</sub> = 10 mA	4.97	5.01	5.05	v v
K <sub>ILIM</sub>	Current programming factor for hardware protection	$R_{LIM} = K_{ILIM} / I_{ILIM}$ , where $I_{ILIM}$ is the hardware current limit. $I_{OUT} = 500 \text{ mA}$	303	314	321	ΑΩ
K <sub>IMAX</sub>	Current programming factor for the nominal operating current	I <sub>IMAX</sub> = K <sub>IMAX</sub> / R <sub>LIM</sub> where I <sub>MAX</sub> is the maximum normal operating current. I <sub>OUT</sub> = 500 mA		262		ΑΩ
I <sub>OUT</sub>	Current limit programming range				750	mA
	Comment limit during MADO	I <sub>OUT</sub> > 300 mA	I,	<sub>OUT</sub> + 50		mA
ICOMM	Current limit during WPC communication	I <sub>OUT</sub> < 300 mA	343	378	425	mA
t <sub>HOLD</sub>	Hold off time for the communication current limit during startup			1		s



# **ELECTRICAL CHARACTERISTICS (continued)**

over operating free-air temperature range, 0°C to 125°C (unless otherwise noted)

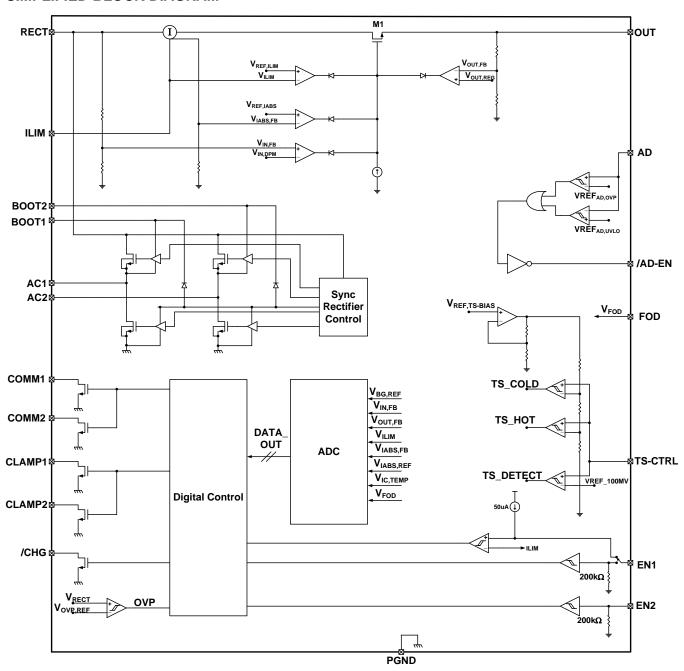
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
TS / CTRL						
$V_{TS}$	Internal TS bias voltage	$I_{TS-Bias}$ < 100 $\mu$ A (periodically driven see $t_{TS-CTRL}$ )	2	2.2	2.4	V
\ /	Rising threshold	V <sub>TS</sub> : 50% → 60%	56.5	58.7	60.8	
V <sub>COLD</sub>	Falling hysteresis	V <sub>TS</sub> : 60% → 50%		2		0/1/
\ /	Falling threshold	V <sub>TS</sub> : 20% → 15%	18.5	19.6	20.7	%V <sub>TS-Bias</sub>
$V_{HOT}$	Rising hysteresis	V <sub>TS</sub> : 15% → 20%		3		
V	CTRL pin threshold for a high	$V_{TS-CTRL}$ : 50 $\rightarrow$ 150 mV	80	100	130	mV
$V_{CTRL}$	CTRL pin threshold for a low	$V_{TS-CTRL}$ : 150 $\rightarrow$ 50 mV	50	80	100	mV
t <sub>TS-CTRL</sub>	Time V <sub>TS</sub> -Bias is active when TS measurements occur	Synchronous to the communication period		24		ms
t <sub>TS</sub>	Deglitch time for all TS comparators			10		ms
R <sub>TS</sub>	Pull-up resistor for the NTC network. Pulled up to the voltage bias.		18	20	22	kΩ
THERMAL PR	ROTECTION				*	
<b>T</b>	Thermal shutdown temperature			155		°C
$T_J$	Thermal shutdown hysteresis			20		°C
OUTPUT LOG	GIC LEVELS ON CHG				'	
V <sub>OL</sub>	Open drain CHG pin	I <sub>SINK</sub> = 5 mA			500	mV
I <sub>OFF</sub>	CHG leakage current when disabled	V <sub>CHG</sub> = 20 V			1	μΑ
COMM PIN						
R <sub>DS(ON)</sub>	COMM1 and COMM2	V <sub>RECT</sub> = 2.6 V		1.5		Ω
f <sub>COMM</sub>	Signaling frequency on COMM pin			2.00		Kb/s
I <sub>OFF</sub>	Comm pin leakage current	V <sub>COMM1</sub> = 20 V, V <sub>COMM2</sub> = 20 V			1	μΑ
CLAMP PIN					,	
R <sub>DS(ON)</sub>	CLAMP1 and CLAMP2			0.8		Ω
ADAPTER EN	IABLE					
\/	V <sub>AD</sub> rising threshold voltage. EN-UVLO	$V_{AD} \ 0 \ V \rightarrow 5 \ V$	3.5	3.6	3.8	V
$V_{\overline{AD-EN}}$	V <sub>AD-EN</sub> hysteresis, EN-HYS	$V_{AD}$ 5 $V \rightarrow 0 V$		400		mV
I <sub>AD</sub>	Input leakage current	V <sub>RECT</sub> = 0 V, V <sub>AD</sub> = 5 V			60	μΑ
R <sub>AD</sub>	Pull-up resistance from $\overline{\text{AD-EN}}$ to OUT when adapter mode is disabled and $V_{\text{OUT}} > V_{\text{AD}}$ , EN-OUT	V <sub>AD</sub> = 0 V, V <sub>OUT</sub> = 5 V		200	350	Ω
$V_{AD}$	Voltage difference between V <sub>AD</sub> and V <sub>AD-EN</sub> when adapter mode is enabled, EN-ON	V <sub>AD</sub> = 5 V, 0°C ≤ T <sub>J</sub> ≤ 85°C	3	4.5	5	V
SYNCHRONO	OUS RECTIFIER					
	I <sub>OUT</sub> at which the synchronous rectifier enters half synchronous mode, SYNC_EN	$I_{LOAD}$ : 200 mA $\rightarrow$ 0 mA	80	100	130	mA
l <sub>OUT</sub>	Hysteresis for I <sub>OUT,RECT-EN</sub> (full-synchronous mode enabled)	$I_{LOAD}$ : 0 mA $\rightarrow$ 200 mA		25		mA
V <sub>HS-DIODE</sub>	High-side diode drop when the rectifier is in half synchronous mode	$I_{AC-VRECT} = 250 \text{ mA}$ and $T_J = 25^{\circ}\text{C}$		0.7		V
EN1 AND EN2	2					
V <sub>IL</sub>	Input low threshold for EN1 and EN2				0.4	V
V <sub>IH</sub>	Input high threshold for EN1 and EN2		1.3			V
R <sub>PD</sub>	EN1 and EN2 pull down resistance			200		kΩ
	elated Measurements and Coefficients)	ı L			L	
IOUT SENSE	Accuracy of the current sense over the load range	I <sub>OUT</sub> = 300 mA - 500 mA	-1.5%	0%	0.9%	

Submit Documentation Feedback

www.ti.com

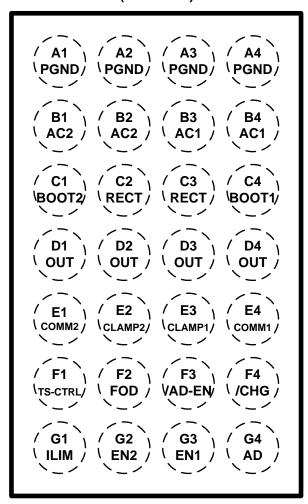
### DEVICE INFORMATION

### SIMPLIFIED BLOCK DIAGRAM





# YFP Package (TOP VIEW)



### **PIN FUNCTIONS**

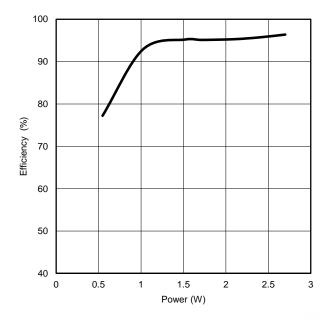
NAME	YFP	I/O	DESCRIPTION
AC1	B3, B4	I	AC insult from second on sell automa
AC2	B1, B2	I	AC input from receiver coil antenna.
BOOT1	C4	0	Bootstrap capacitors for driving the high-side FETs of the synchronous rectifier. Connect a 10 nF ceramic
BOOT2	C1	0	capacitor from BOOT1 to AC1 and from BOOT2 to AC2.
RECT	C2, C3	0	Filter capacitor for the internal synchronous rectifier. Connect a ceramic capacitor to PGND. Depending on the power levels, the value may be 4.7 $\mu$ F to 22 $\mu$ F.
OUT	D1, D2, D3, D4	0	Output pin, delivers power to the load.
COMM1	E4	0	Open-drain output used to communicate with primary by varying reflected impedance. Connect COMM1
COMM2	E1	0	through a capacitor to either AC1 or AC2 for capacitive load modulation (COMM2 must be connected to the alternate AC1 or AC2 pin). For resistive modulation connect COMM1 and COMM2 to RECT via a single resistor; connect through separate capacitors for capacitive load modulation.
CLAMP2	E2	0	Open drain FETs which are utilized for a non-power dissipative over-voltage AC clamp protection. When the
CLAMP1	E3	0	RECT voltage goes above 15 V, both switches will be turned on and the capacitors will act as a low impedance to protect the IC from damage. If used, CLAMP1 is required to be connected to AC1, and CLAMP2 is required to be connected to AC2 via 0.47 µF capacitors.
PGND	A1, A2, A3, A4		Power ground



# **PIN FUNCTIONS (continued)**

NAME	YFP	I/O	DESCRIPTION
ILIM	G1	I/O	Programming pin for the over current limit. Connect external resistor to VSS. Size $R_{ILIM}$ with the following equation: $R_{ILIM} = 250 / I_{MAX}$ where $I_{MAX}$ is the expected maximum output current of the wireless power supply. The hardware current limit ( $I_{ILIM}$ ) will be 20% greater than $I_{MAX}$ or 1.2 x $I_{MAX}$ . If the supply is meant to operate in current limit use $R_{ILIM} = 314 / I_{ILIM}$ $R_{ILIM} = R1 + R_{FOD}$
AD	G4	I	Connect this pin to the wired adapter input. When a voltage is applied to this pin wireless charging is disabled and $\overline{AD\_EN}$ is driven low. Connect to GND through a 1 $\mu F$ capacitor. If unused, capacitor is not required and should be grounded directly.
AD-EN	F3	0	Push-pull driver for external PFET connecting AD and OUT. This node is pulled to the higher of OUT and AD when turning off the external FET. This voltage tracks approximately 4 V below AD when voltage is present at AD and provides a regulated $V_{\rm GS}$ bias for the external FET. Float this pin if unused.
TS-CTRL	F1	1	Must be connected to ground via a resistor. If an NTC function is not desired connect to GND with a $10\text{-}k\Omega$ resistor. As a CTRL pin pull to ground to send end power transfer (EPT) fault to the transmitter or pull-up to an internal rail (i.e. 1.8 V) to send EPT termination to the transmitter. Note that a 3-state driver should be used to interface this pin (see the 3-state Driver section for further description).
EN1	G3	ı	Inputs that allow user to enable/disable wireless and wired charging <en1 en2="">:</en1>
EN2	G2	I	<00> Wireless charging is enabled <01> Dynamic communication current limit disabled <10> Wireless charging disabled <11> Wireless charging disabled.
FOD	F2	I	Input for the recieved power measurement. Connect to GND with a R <sub>FOD</sub> resistor.
CHG	F4	0	Open-drain output – Active when the output of the wireless power supply is enabled.

### TYPICAL CHARACTERISTICS





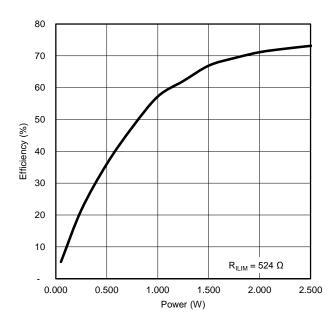
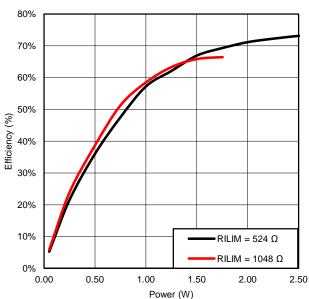


Figure 5. System Efficiency from DC Input to DC Output



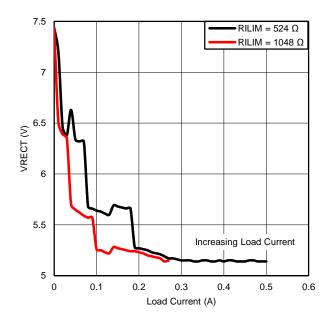
### **TYPICAL CHARACTERISTICS (continued)**



Load Current Rising Load Current Falling 7 6.5 VRECT (V) 6  $R_{ILIM} = 524 \Omega$ 5.5 5 0.1 0.3 0.6 0 0.2 0.4 0.5 Load Current (A)

Figure 6. Light Load System Efficiency Improvement Due to Dynamic Efficiency Scaling Feature

Figure 7.  $V_{RECT}$  vs.  $I_{LOAD}$  at  $R_{ILIM}$  = 524  $\Omega$ 



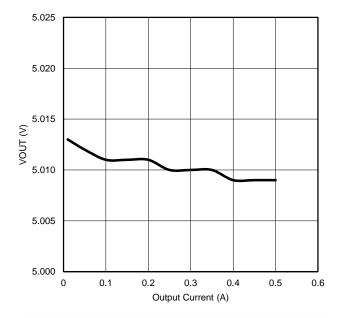
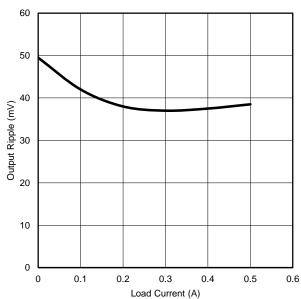


Figure 8.  $V_{RECT}$  vs.  $I_{LOAD}$  at  $R_{ILIM}$  = 524  $\Omega$  and 1048  $\Omega$ 

Figure 9. I<sub>LOAD</sub> Sweep (I-V Curve)

# **TYPICAL CHARACTERISTICS (continued)**



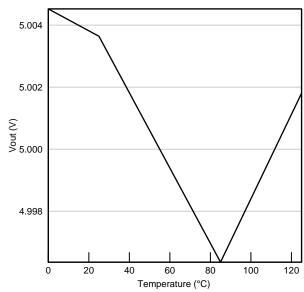


Figure 10. Output Ripple vs.  $I_{LOAD}$  ( $C_{OUT}$  = 1  $\mu$ F) without Communication

Figure 11.  $V_{OUT}$  vs Temperature

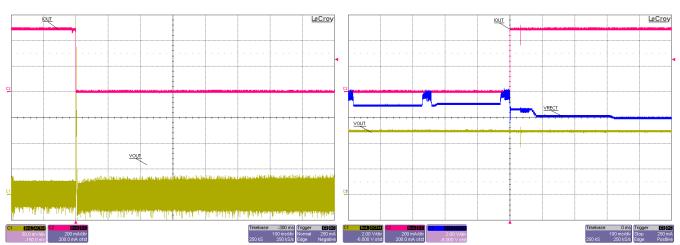


Figure 12. 0.5-A Instantaneous Load Dump

Figure 13. 0.5-A Load Step Full System Response





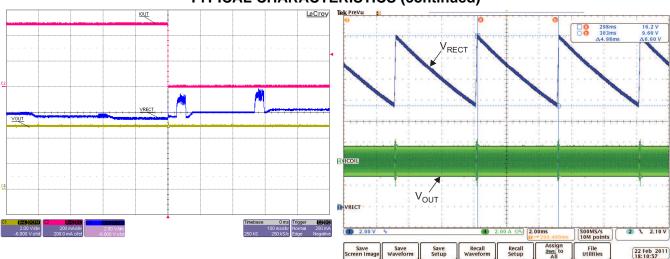


Figure 14. 0.5-A Load Dump Full System Response

Figure 15. Rectifier Overvoltage Clamp ( $f_{op} = 110 \text{ kHz}$ )

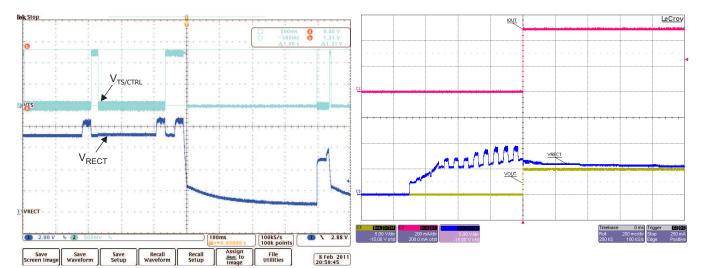


Figure 16. TS Fault

Figure 17. Typical Startup with a 0.5-A System Load

Submit Documentation Feedback



### TYPICAL CHARACTERISTICS (continued)

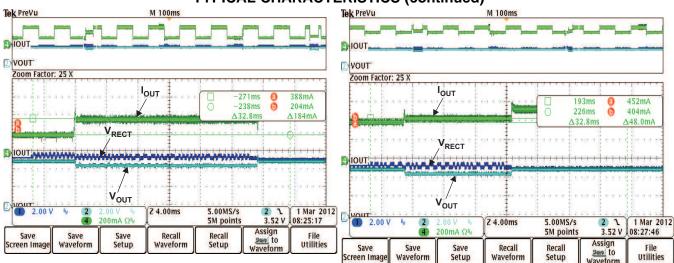


Figure 18. Adaptive Communication Limit Event Where the 400-mA Current Limit is Enabled ( $I_{OUT-DC}$  < 300 mA)

Figure 19. Adaptive Communication Limit Event Where the Current Limit is  $I_{\rm OUT}$  + 50 mA ( $I_{\rm OUT-DC}$  > 300 mA)

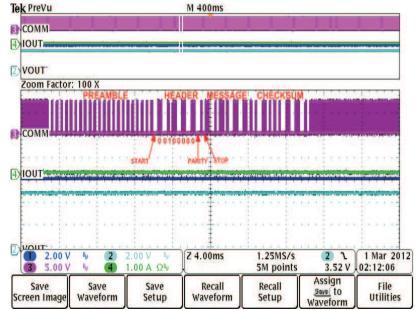


Figure 20. Rx Communication Packet Structure



#### PRINCIPLE OF OPERATION

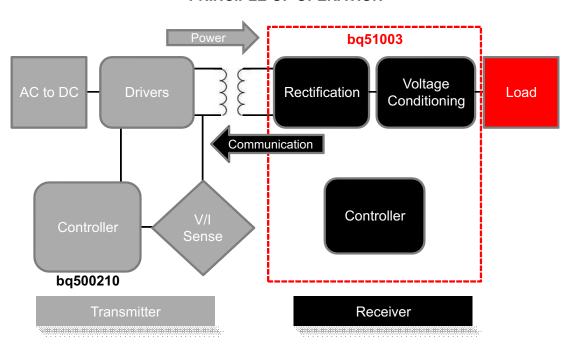


Figure 21. WPC Wireless Power System Indicating the Functional Integration of the bq51003

### A Brief Description of the Wireless System:

A wireless system consists of a charging pad (transmitter or primary) and the secondary-side equipment (receiver or secondary). There is a coil in the charging pad and in the secondary equipment which are magnetically coupled to each other when the secondary is placed on the primary. Power is then transferred from the transmitter to the receiver via coupled inductors (e.g. an air-core transformer). Controlling the amount of power transferred is achieved by sending feedback (error signal) communication to the primary (that is, to increase or decrease power).

The receiver communicates with the transmitter by changing the load seen by the transmitter. This load variation results in a change in the transmitter coil current, which is measured and interpreted by a processor in the charging pad. The communication is digital - packets are transferred from the receiver to the transmitter. Differential Bi-phase encoding is used for the packets. The bit rate is 2-kbps.

Various types of communication packets have been defined. These include identification and authentication packets, error packets, control packets, end power packets, and power usage packets.

The transmitter coil stays powered off most of the time. It occasionally wakes up to see if a receiver is present. When a receiver authenticates itself to the transmitter, the transmitter will remain powered on. The receiver maintains full control over the power transfer using communication packets.

### Using the bq51003 as a Wireless Power Supply: (See Figure 2)

Figure 2 is the schematic of a system which uses the bq51003 as a power supply.

When the system shown in Figure 2 is placed on the charging pad, the receiver coil is inductively coupled to the magnetic flux generated by the coil in the charging pad which consequently induces a voltage in the receiver coil. The internal synchronous rectifier feeds this voltage to the RECT pin which has the filter capacitor C3.

Submit Documentation Feedback



The bq51003 identifies and authenticates itself to the primary using the COM pins by switching on and off the COM FETs and hence switching in and out  $C_{COMM}$ . If the authentication is successful, the transmitter will remain powered on. The bq51003 measures the voltage at the RECT pin, calculates the difference between the actual voltage and the desired voltage  $V_{RECT-REG}$ , (threshold 1 at no load) and sends back error packets to the primary. This process goes on until the input voltage settles at  $V_{RECT-REG}$ . During a load transient, the dynamic rectifier algorithm will set the targets specified by  $V_{RECT-REG}$  thresholds 1, 2, 3, and 4. This algorithm is termed Dynamic Rectifier Control and is used to enhance the transient response of the power supply.

During power-up, the LDO is held off until the  $V_{RECT-REG}$  threshold 1 converges. The voltage control loop ensures that the output voltage is maintained at  $V_{OUT-REG}$  to power the system. The bq51003 meanwhile continues to monitor the input voltage, and maintains sending error packets to the primary every 250 ms. If a large overshoot occurs, the feedback to the primary speeds up to every 32 ms in order to converge on an operating point in less time.

### Details of a Qi Wireless Power System and bq51003 Power Transfer Flow Diagrams

The bq51003 integrates a fully compliant WPC v1.1 communication algorithm in order to streamline receiver designs (no extra software development required). Other unique algorithms such as Dynamic Rectifier Control are also integrated to provide best-in-class system performance. This section provides a high level overview of these features by illustrating the wireless power transfer flow diagram from startup to active operation.

During startup operation, the wireless power receiver must comply with proper handshaking to be granted a power contract from the Tx. The Tx will initiate the hand shake by providing an extended digital ping. If an Rx is present on the Tx surface, the Rx will then provide the signal strength, configuration and identification packets to the Tx (see volume 1 of the WPC specification for details on each packet). These are the first three packets sent to the Tx. The only exception is if there is a true shutdown condition on the EN1/EN2, AD, or TS-CTRL pins where the Rx will shut down the Tx immediately. See Table 4 for details. Once the Tx has successfully received the signal strength, configuration and identification packets, the Rx will be granted a power contract and is then allowed to control the operating point of the power transfer. With the use of the bq51003 Dynamic Rectifier Control algorithm, the Rx will inform the Tx to adjust the rectifier voltage above 7 V prior to enabling the output supply. This method enhances the transient performance during system startup. See Figure 22 for the startup flow diagram details.

Product Folder Links: bq51003



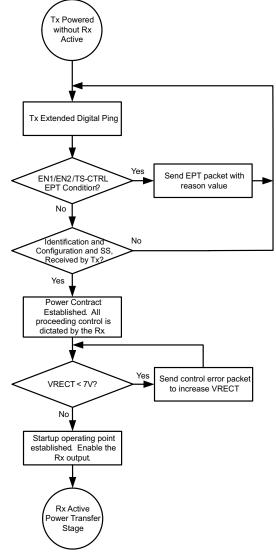


Figure 22. Wireless Power Startup Flow Diagram

Once the startup procedure has been established, the Rx will enter the active power transfer stage. This is considered the "main loop" of operation. The Dynamic Rectifier Control algorithm will determine the rectifier voltage target based on a percentage of the maximum output current level setting (set by K<sub>IMAX</sub> and the ILIM resistance to GND). The Rx will send control error packets in order to converge on these targets. As the output current changes, the rectifier voltage target will dynamically change. As a note, the feedback loop of the WPC system is relatively slow where it can take up to 90 ms to converge on a new rectifier voltage target. It should be understood that the instantaneous transient response of the system is open loop and dependent on the Rx coil output impedance at that operating point. More details on this will be covered in the section Receiver Coil Load-Line Analysis. The "main loop" will also determine if any conditions in Table 4 are true in order to discontinue power transfer. See Figure 23 which illustrates the active power transfer loop.

SLUSBC8 - DECEMBER 2013

www.ti.com

Rx Active Power Transfer Stage Rx Shutdown Tx Powered Yes Send EPT packet with conditions per the EP without Rx reason value Table? Active No VRECT target = 7V. Send Yes IOUT < 10% of IMAX? control error packets to converge. No VRECT target = 6.3V. IOUT < 20% of IMAX? end control error packe to converge No VRECT target = 5.5V. Yes IOUT < 40% of IMAX? Send control error packe to converge No VRECT target= 5.1V. Send control error packet to converge. Measure Rectified Power and Send Value to Tx

Figure 23. Active Power Transfer Flow Diagram

Another requirement of the WPC v1.1 specification is to send the measured recieved power. This task is enabled on the IC by measuring the voltage on the FOD pin which is proportional to the output current and can be scaled based on the choice of the resitor to ground on the FOD pin.

### **Dynamic Rectifier Control**

The Dynamic Rectifier Control algorithm offers the end system designer optimal transient response for a given max output current setting. This is achieved by providing enough voltage headroom across the internal regulator at light loads in order to maintain regulation during a load transient. The WPC system has a relatively slow global feedback loop where it can take more than 90 ms to converge on a new rectifier voltage target. Therefore, the transient response is dependent on the loosely coupled transformers output impedance profile. The Dynamic Rectifier Control allows for a 2 V change in rectified voltage before the transient response will be observed at the output of the internal regulator (output of the bg51003).



### **Dynamic Efficiency Scaling**

The Dynamic Efficiency Scaling feature allows for the loss characteristics of the bq51003 to be scaled based on the maximum expected output power in the end application. This effectively optimizes the efficiency for each application. This feature is achieved by scaling the loss of the internal LDO based on a percentage of the maximum output current. Note that the maximum output current is set by the  $K_{IMAX}$  term and the  $R_{ILIM}$  resistance (where  $R_{ILIM} = K_{IMAX} / I_{MAX}$ ). The flow diagram show in Figure 23 illustrates how the rectifier is dynamically controlled (*Dynamic Rectifier Control*) based on a fixed percentage of the  $I_{MAX}$  setting. Table 1 summarizes how the rectifier behavior is dynamically adjusted based on two different  $R_{ILIM}$  settings.

Table 1.

OUTPUT CURRENT PERCENTAGE	$R_{ILIM}$ = 1116 Ω $I_{MAX}$ = 250 mA	R <sub>ILIM</sub> = 488 Ω I <sub>MAX</sub> = 500 mA	V <sub>RECT</sub>
0 to 10%	0 A to 0.025 A	0 A to 0.05 A	7.08 V
10 to 20%	0.025 A to 0.050 A	0.050 A to 0.100 A	6.28 V
20 to 40%	0.050 A to 0.100 A	0.100 A to 0.200 A	5.53 V
>40%	> 0.100 A	> 0.200 A	5.11 V

Figure 8 illustrates the shift in the *Dynamic Rectifier Control* behavior based on the two different R<sub>ILIM</sub> settings. With the rectifier voltage (V<sub>RECT</sub>) being the input to the internal LDO, this adjustment in the *Dynamic Rectifier Control* thresholds will dynamically adjust the power dissipation across the LDO where:

$$P_{DIS} = (V_{RECT} - V_{OUT}) \times I_{OUT}$$
(1)

Figure 6 illustrates how the system efficiency is improved due to the *Dynamic Efficiency Scaling* feature. Note that this feature balances efficiency with optimal system transient response.

### R<sub>ILIM</sub> Calculations

The bq51003 includes a means of providing hardware overcurrent protection by means of an analog current regulation loop. The hardware current limit provides an extra level of safety by clamping the maximum allowable output current (that is, a current compliance). The  $R_{\rm ILIM}$  resistor size also sets the thresholds for the dynamic rectifier levels and thus providing efficiency tuning per each application's maximum system current. The calculation for the total  $R_{\rm ILIM}$  resistance is as follows:

$$R_{ILIM} = \frac{262}{I_{MAX}}$$

$$I_{ILIM} = 1.2 \times I_{MAX} = \frac{314}{R_{ILIM}}$$

$$R_{ILIM} = R_1 + R_{FOD}$$
(2)

Where  $I_{MAX}$  is the expected maximum output current during normal operation and  $I_{ILIM}$  is the hardware over current limit. When referring to the application diagram shown in Figure 2,  $R_{ILIM}$  is the sum of  $R_{FOD}$  and the  $R_1$  resistance (that is, the total resistance from the ILIM pin to GND).

#### Input Overvoltage

If the input voltage suddenly increases in potential (that is, due to a change in position of the equipment on the charging pad), the voltage-control loop inside the bq51003 becomes active, and prevents the output from going beyond  $V_{OUT-REG}$ . The receiver then starts sending back error packets to the transmitter every 30 ms until the input voltage comes back to the  $V_{RECT-REG}$  target, and then maintains the error communication every 250 ms.

If the input voltage increases in potential beyond  $V_{RECT-OVP}$ , the IC switches off the LDO and communicates to the primary to bring the voltage back to  $V_{RECT-REG}$ . In addition, a proprietary voltage protection circuit is activated by means of  $C_{CLAMP1}$  and  $C_{CLAMP2}$  that protects the IC from voltages beyond the maximum rating of the IC (that is, 20 V).

Submit Documentation Feedback

### Adapter Enable Functionality and EN1/EN2 Control

Figure 3 is an example application that shows the bq51003 used as a wireless power receiver that can power mutiplex between wired or wireless power for the down-system electronics. In the default operating mode pins EN1 and EN2 are low, which activates the adapter enable functionality. In this mode, if an adapter is not present the AD pin will be low, and  $\overline{AD}$ -EN pin will be pulled to the higher of the OUT and AD pins so that the PMOS between OUT and AD will be turned off. If an adapter is plugged in and the voltage at the AD pin goes above 3.6 V then wireless charging is disabled and the  $\overline{AD}$ -EN pin will be pulled approximately 4 V below the AD pin to connect AD to the secondary charger. The difference between AD and  $\overline{AD}$ -EN is regulated to a maximum of 7 V to ensure the  $V_{GS}$  of the external PMOS is protected.

The EN1 and EN2 pins include internal 200-k $\Omega$  pull-down resistors, so that if these pins are not connected bq51003 defaults to  $\overline{\text{AD-EN}}$  control mode. However, these pins can be pulled high to enable other operating modes as described in Table 2:

#### Table 2.

EN1	EN2	RESULT
0	0	Adapter control enabled. If adapter is present then secondary charger is powered by adapter, otherwise wireless charging is enabled when wireless power is available. Communication current limit is enabled.
0	1	Disables communication current limit.
1	0	AD-EN is pulled low, whether or not adapter voltage is present. This feature can be used, e.g., for USB OTG applications.
1	1	Adapter and wireless charging are disabled, i.e., power will never be delivered by the OUT pin in this mode.

#### Table 3.

EN1	EN2	WIRELESS POWER	WIRED POWER	OTG MODE	ADAPTIVE COMMUNICATION LIMIT	EPT
0	0	Enabled	Priority <sup>(1)</sup>	Disabled	Enabled	Not Sent to Tx
0	1	Priority <sup>(1)</sup>	Enabled	Disabled	Disabled	Not Sent to Tx
1	0	Disabled	Enabled	Enabled <sup>(2)</sup>	N/A	No Response
1	1	Disabled	Disabled	Disabled	N/A	Termination

<sup>(1)</sup> If both wired and wireless power are present, wired power is given priority.

As described in Table 3, pulling EN2 high disables the adapter mode and only allows wireless charging. In this mode the adapter voltage will always be blocked from the OUT pin. An application example where this mode is useful is when USB power is present at AD, but the USB is in suspend mode so that no power can be taken from the USB supply. Pulling EN1 high enables the off-chip PMOS regardless of the presence of a voltage. This function can be used in USB OTG mode to allow a charger connected to the OUT pin to power the AD pin. Finally, pulling both EN1 and EN2 high disables both wired and wireless charging.

#### **NOTE**

It is required to connect a back-to-back PMOS between AD and OUT so that voltage is blocked in both directions. Also, when AD mode is enabled no load can be pulled from the RECT pin as this could cause an internal device overvoltage in bq51003.

### **End Power Transfer Packet (WPC Header 0x02)**

The WPC allows for a special command for the receiver to terminate power transfer from the transmitter termed End Power Transfer (EPT) packet. Table 4 specifies the v1.1 reasons column and their corresponding data field value. The condition column corresponds to the methodology used by bg51003 to send equivalent message.

Product Folder Links: bq51003

<sup>(2)</sup> Allows for a boost-back supply to be driven from the output terminal of the Rx to the adapter port via the external back-to-back PMOS FET.

#### Table 4.

MESSAGE	VALUE	CONDITION
Charge Complete	0x01	TS-CTRL = 1, or EN1 = 1, or <en1 en2=""> = &lt;11&gt;</en1>
Internal Fault	0x02	$T_J > 150$ °C or $R_{ILIM} < 100 \Omega$
Over Temperature	0x03	TS < $V_{HOT}$ , TS > $V_{COLD}$ , or TS-CTRL < 100 mV
Over Voltage	0x04	Not Sent
Over Current	0x05	NOT USED
Battery Failure	0x06	Not Sent
Reconfigure	0x07	Not Sent
No Response	0x08	V <sub>RECT</sub> target does not converge

### **Status Outputs**

The bq51003 has one status output,  $\overline{\text{CHG}}$ . This output is an open-drain NMOS device that is rated to 20 V. The open-drain FET connected to the  $\overline{\text{CHG}}$  pin will be turned on whenever the output of the power supply is enabled. Please note, the output of the power supply will not be enabled if the  $V_{\text{RECT-REG}}$  does not converge at the no-load target voltage.

#### **WPC Communication Scheme**

The WPC communication uses a modulation technique termed "backscatter modulation" where the receiver coil is dynamically loaded in order to provide amplitude modulation of the transmitter's coil voltage and current. This scheme is possible due to the fundamental behavior between two loosely coupled inductors (that is, between the Tx and Rx coil). This type of modulation can be accomplished by switching in and out a resistor at the output of the rectifier, or by switching in and out a capacitor across the AC1/AC2 net. Figure 24 shows how to implement resistive modulation.

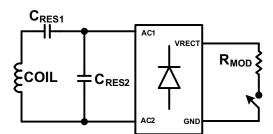


Figure 24. Resistive Modulation

Figure 25 shows how to implement capacitive modulation.

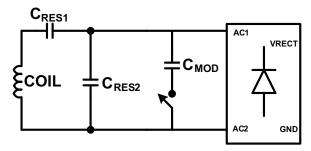


Figure 25. Capacitive Modulation

20 Submi

The amplitude change in Tx coil voltage or current can be detected by the transmitters decoder. The resulting signal observed by the Tx is shown in Figure 26.

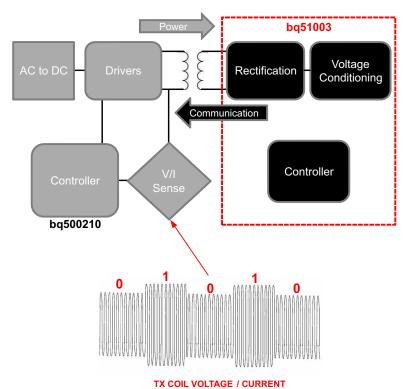


Figure 26.

The WPC protocol uses a differential bi-phase encoding scheme to modulate the data bits onto the Tx coil voltage/current. Each data bit is aligned at a full period of 0.5 ms ( $t_{CLK}$ ) or 2 kHz. An encoded ONE results in two transitions during the bit period and an encoded ZERO results in a single transition. See Figure 27 for an example of the differential bi-phase encoding.

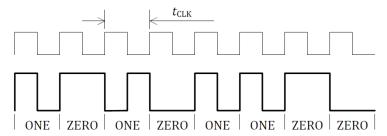


Figure 27. Differential Bi-phase Encoding Scheme (WPC Volume 1: Low Power, Part 1 Interface Definition)

The bits are sent LSB first and use an 11-bit asynchronous serial format for each portion of the packet. This includes one start bit, n-data bytes, a parity bit, and a single stop bit. The start bit is always ZERO and the parity bit is odd. The stop bit is always ONE. Figure 28 shows the details of the asynchronous serial format.

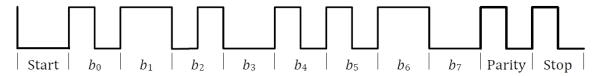


Figure 28. Asynchronous Serial Formatting (WPC volume 1: Low Power, Part 1 Interface Definition)



Each packet format is organized as shown in Figure 29.



Figure 29. Packet Format (WPC Volume 1: Low Power, Part 1 Interface Definition)

Figure 20 above shows an example waveform of the receiver sending a rectified power packet (header 0x04).

#### **Communication Modulator**

The bq51003 provides two identical, integrated communication FETs which are connected to the pins COMM1 and COMM2. These FETs are used for modulating the secondary load current which allows bq51003 to communicate error control and configuration information to the transmitter. Figure 30 shows how the COMM pins can be used for resistive load modulation. Each COMM pin can handle at most a 24- $\Omega$  communication resistor. Therefore, if a COMM resistor between 12  $\Omega$  and 24  $\Omega$  is required COMM1 and COMM2 pins must be connected in parallel. The bq51003 does not support a COMM resistor less than 12  $\Omega$ .

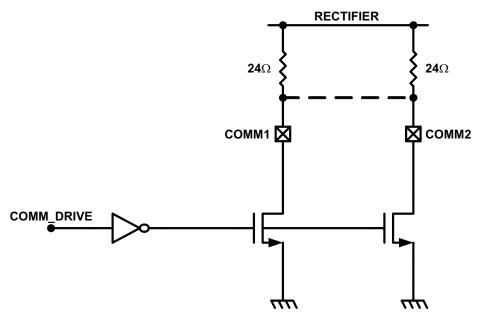


Figure 30. Resistive Load Modulation

In addition to resistive load modulation, the bq51003 is also capable of capacitive load modulation as shown in Figure 31. In this case, a capacitor is connected from COMM1 to AC1 and from COMM2 to AC2. When the COMM switches are closed there is effectively a 22 nF capacitor connected between AC1 and AC2. Connecting a capacitor in between AC1 and AC2 modulates the impedance seen by the coil, which will be reflected in the primary as a change in current.

22

SLUSBC8 - DECEMBER 2013

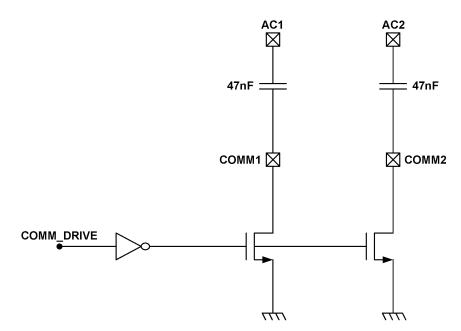


Figure 31. Capacitive Load Modulation

### **Adaptive Communication Limit**

www.ti.com

The Qi communication channel is established via backscatter modulation as described in the previous sections. This type of modulation takes advantage of the loosely coupled inductor relationship between the Rx and Tx coil. Essentially the switching in-and-out of the communication capacitor or resistor adds a transient load to the Rx coil in order to modulate the Tx coil voltage/current waveform (amplitude modulation). The consequence of this technique is that a load transient (load current noise) from the mobile device has the same signature. In order to provide noise immunity to the communication channel, the output load transients must be isolated from the Rx coil. The proprietary feature Adaptive Communication Limit achieves this by dynamically adjusting the current limit of the regulator. When the regulator is put in current limit, any load transients will be offloaded to the battery in the system.

Note that this requires the battery charger IC to have input voltage regulation (weak adapter mode). The output of the Rx appears as a weak supply if a transient occurs above the current limit of the regulator.

The Adaptive Communication Limit feature has two current limit modes and is detailed in Table 5:

Table 5.

I <sub>оит</sub>	COMMUNICATION CURRENT LIMIT				
< 300 mA	Fixed 400 mA				
> 300 mA	I <sub>OUT</sub> + 50 mA				

#### **Synchronous Rectification**

The bq51003 provides an integrated, self-driven synchronous rectifier that enables high-efficiency AC to DC power conversion. The rectifier consists of an all NMOS H-Bridge driver where the backgates of the diodes are configured to be the rectifier when the synchronous rectifier is disabled. During the initial startup of the WPC system the synchronous rectifier is not enabled. At this operating point, the DC rectifier voltage is provided by the diode rectifier. Once V<sub>RECT</sub> is greater than UVLO, half synchronous mode will be enabled until the load current surpasses 120 mA. Above 120 mA the full synchronous rectifier stays enabled until the load current drops back below 100 mA where half synchronous mode is enabled instead.

Product Folder Links: bq51003

### **Temperature Sense Resistor Network (TS)**

bq51003 includes a ratiometric external temperature sense function. The temperature sense function has two ratiometric thresholds which represent a hot and cold condition. An external temperature sensor is recommended in order to provide safe operating conditions for the receiver product. This pin is best used for monitoring the surface that can be exposed to the end user (that is, place the NTC resistor closest to the user).

Figure 32 allows for any NTC resistor to be used with the given V<sub>HOT</sub> and V<sub>COLD</sub> thresholds.

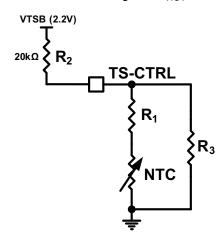


Figure 32. NTC Circuit Used for Safe Operation of the Wireless Receiver Power Supply

The resistors  $R_1$  and  $R_3$  can be solved by resolving the system of equations at the desired temperature thresholds. The two equations are:

$$\%V_{\text{COLD}} = \frac{\left(\frac{R_{3} \left(R_{\text{NTC}}|_{\text{TCOLD}} + R_{1}\right)}{R_{3} + \left(R_{\text{NTC}}|_{\text{TCOLD}} + R_{1}\right)} \times 100}{\left(\frac{R_{3} \left(R_{\text{NTC}}|_{\text{TCOLD}} + R_{1}\right)}{R_{3} + \left(R_{\text{NTC}}|_{\text{TCOLD}} + R_{1}\right)} + R2} \times 100}$$

$$\%V_{\text{HOT}} = \frac{\left(\frac{R_{3} \left(R_{\text{NTC}}|_{\text{THOT}} + R_{1}\right)}{R_{3} + \left(R_{\text{NTC}}|_{\text{THOT}} + R_{1}\right)} \times 100}{\left(\frac{R_{3} \left(R_{\text{NTC}}|_{\text{THOT}} + R_{1}\right)}{R_{3} + \left(R_{\text{NTC}}|_{\text{THOT}} + R_{1}\right)} + R2}\right)} \times 100}$$

$$(3)$$

Where:

$$R_{\text{NTC}}|_{\text{TCOLD}} = R_{0}e^{\beta\left(\frac{1}{T_{\text{TCOLD}}} - \frac{1}{T_{0}}\right)}$$

$$R_{\text{NTC}}|_{\text{THOT}} = R_{0}e^{\beta\left(\frac{1}{T_{\text{HOT}}} - \frac{1}{T_{0}}\right)}$$
(4)

where,  $T_{COLD}$  and  $T_{HOT}$  are the desired temperature thresholds in degrees Kelvin.  $R_O$  is the nominal resistance and  $\beta$  is the temperature coefficient of the NTC resistor.  $R_O$  is fixed at 20 k $\Omega$ . An example solution is provided:

- R1 =  $4.23 \text{ k}\Omega$
- R3 = 66.8  $k\Omega$

where the chosen parameters are:

- $%V_{HOT} = 19.6\%$
- $%V_{COLD} = 58.7\%$
- $T_{COLD} = -10^{\circ}C$

24

STRUMENTS

- T<sub>HOT</sub> = 100°C
- $\beta = 3380$
- R<sub>O</sub> = 10 kΩ

The plot of the percent  $V_{TSB}$  vs. temperature is shown in Figure 33:

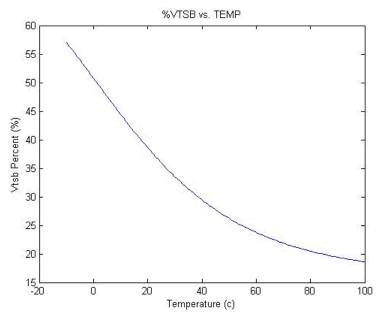


Figure 33. Example Solution for an NTC resistor with  $R_0$  = 10  $k\Omega$  and  $\beta$  = 4500

Figure 34 illustrates the periodic biasing scheme used for measuring the TS state. The TS\_READ signal enables the TS bias voltage for 24 ms. During this period the TS comparators are read (each comparator has a 10-ms deglitch) and appropriate action is taken based on the temperature measurement. After this 24-ms period has elapsed, the TS\_READ signal goes low, which causes the TS-Bias pin to become high impedance. During the next 35 ms (priority packet period) or 235 ms (standard packet period), the TS voltage is monitored and compared to 100 mV. If the TS voltage is greater than 100 mV then a secondary device is driving the TS-CTRL pin and a CTRL = '1' is detected.

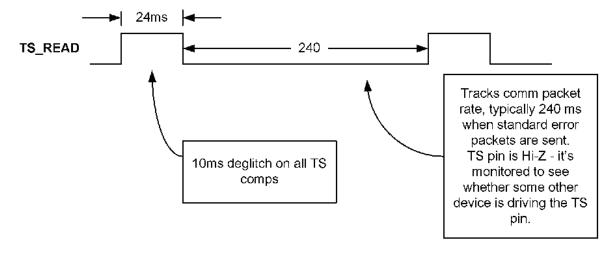


Figure 34. Timing Diagram for TS Detection Circuit

### 3-State Driver Recommendations for the TS-CTRL Pin

The TS-CTRL pin offers three functions with one 3-state driver interface

- 1. NTC temperature monitoring,
- 2. Fault indication,
- 3. Charge done indication

A 3-state driver can be implemented with the circuit in Figure 35 and the use of two GPIO connections.

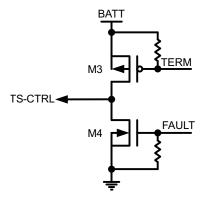


Figure 35. 3-State Driver for TS-CTRL

Note that the signals "TERM" and "FAULT" are given by two GPIOs. The truth table for this circuit is found in Table 6:

Table 6.

TERM	FAULT	F (Result)
1	0	Z (Normal Mode)
0	0	Charge Complete
1	1	System Fault

The default setting is TERM = 1 and FAULT = 0. In this condition, the TS-CTRL net is high impedance (hi-z) and; therefore, the NTC is function is allowed to operate. When the TS-CTRL pin is pulled to GND by setting FAULT = 1, the Rx is shut down with the indication of a fault. When the TS-CTRL pin is pulled to the battery by setting TERM = 1, the Rx is shut down with the indication of a charge complete condition. Therefore, the host controller can indicate whether the Rx is system is turning off due to a fault or due to a charge complete condition.

#### Thermal Protection

The bq51003 includes a thermal shutdown protection. If the die temperature reaches T<sub>1</sub>(OFF), the LDO is shut off to prevent any further power dissipation. In this case bq51003 will send an EPT message of internal fault (0x02).

#### WPC v1.1 Compliance – Foreign Object Detection

The bq51003 is a WPC v1.1 compatible device. In order to enable a Power Transmitter to monitor the power loss across the interface as one of the possible methods to limit the temperature rise of Foreign Objects, the bq51003 reports its Received Power to the Power Transmitter. The Received Power equals the power that is available from the output of the Power Receiver plus any power that is lost in producing that output power (the power loss in the Secondary Coil and series resonant capacitor, the power loss in the Shielding of the Power Receiver, the power loss in the rectifier). In WPC v1.1 specification, foreign object detection (FOD) is enforced. This means the bq51003 will send received power information with known accuracy to the transmitter.

WPC v1.1 defines Received Power as "the average amount of power that the Power Receiver receives through its Interface Surface, in the time window indicated in the Configuration Packet".

Product Folder Links: bq51003

26

Copyright © 2013, Texas Instruments Incorporated

**ISTRUMENTS** 

In order to receive certification as a WPC v1.1 receiver, the Device Under Test (DUT) is tested on a Reference Transmitter whose transmitted power is calibrated, the receiver must send a received power such that:

$$0 \text{ mW} < (Tx PWR)_{REF} - (Rx PWR \text{ out})_{DUT} < -250 \text{ mW}$$
(5)

This 250-mW bias ensures that system will remain interoperable.

WPC v1.1 Transmitter will be tested to see if they can detect reference Foreign Objects with a Reference receiver.

WPC v1.1 Specification will allow much more accurate sensing of Foreign Objects.

### **Series and Parallel Resonant Capacitor Selection**

Shown in Figure 2, the capacitors C1 (series) and C2 (parallel) make up the dual resonant circuit with the receiver coil. These two capacitors must be sized correctly per the WPC v1.1 specification. Figure 36 illustrates the equivalent circuit of the dual resonant circuit:

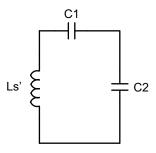


Figure 36. Dual Resonant Circuit with the Receiver Coil

Section 4.2 (Power Receiver Design Requirements) in Part 1 of the WPC v1.1 specification highlights in detail the sizing requirements. To summarize, the receiver designer will be required take inductance measurements with a fixed test fixture. The test fixture is shown in Figure 37:

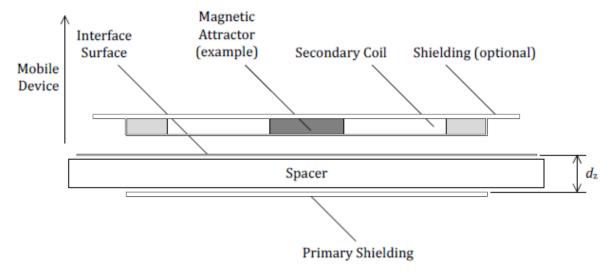


Figure 37. WPC v1.1 Receiver Coil Test Fixture for the Inductance Measurement Ls' (Copied from System Description Wireless Power Transfer, Volume 1: Low Power, Part 1 Interface Definition, Version 1.1)

Product Folder Links: *bq51003* 



The primary shield is to be 50 mm x 50 mm x 1 mm of Ferrite material PC44 from TDK Corp. The gap  $d_Z$  is to be 3.4 mm. The receiver coil, as it will be placed in the final system (that is, the back cover and battery must be included if the system calls for this), is to be placed on top of this surface and the inductance is to be measured at 1-V RMS and a frequency of 100 kHz. This measurement is termed Ls'. The same measurement is to be repeated without the test fixture shown in Figure 37. This measurement is termed Ls or the free-space inductance. Each capacitor can then be calculated using Equation 6:

$$C_{1} = \left[ \left( f_{S} \cdot 2\pi \right)^{2} \cdot L_{S}' \right]^{-1}$$

$$C_{2} = \left[ \left( f_{D} \cdot 2\pi \right)^{2} \cdot L_{S}' - \frac{1}{C_{1}} \right]^{-1}$$
(6)

Where  $f_S$  is 100 kHz +5/-10% and  $f_D$  is 1 MHz ±10%. C1 must be chosen first prior to calculating C2.

The quality factor must be greater than 77 and can be determined by Equation 7:

$$Q = \frac{2\pi \cdot f_{D} \cdot L_{S}}{R} \tag{7}$$

Where R is the DC resistance of the receiver coil. All other constants are defined above.

### **Package Summary**

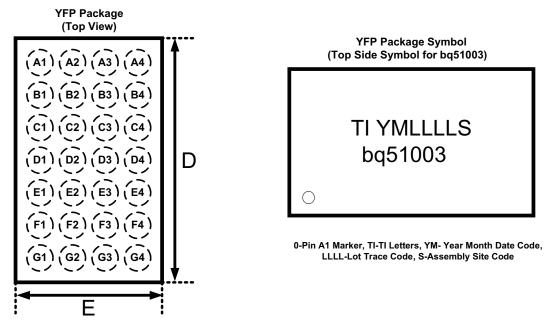


Figure 38. Chip Scale Packaging Dimensions

- $D = 3.0 \text{ mm} \pm 0.035 \text{ mm}$
- E = 1.88 mm ± 0.035 mm

28



### PACKAGE OPTION ADDENDUM

31-Dec-2013

#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
BQ51003YFPR	ACTIVE	DSBGA	YFP	28	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	BQ51003	Samples
BQ51003YFPT	ACTIVE	DSBGA	YFP	28	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	BQ51003	Samples

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

- (3) MSL, Peak Temp. The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
- (4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
- (5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
- (6) Lead/Ball Finish Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.



# **PACKAGE OPTION ADDENDUM**

31-Dec-2013

n no event shall TI's liability arising out of such information ex	xceed the total purchase price of the TI part(s) at issue	in this document sold by TI to Customer on an annual basis.
--	---	---

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 17-Jun-2015

### TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
BQ51003YFPR	DSBGA	YFP	28	3000	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51003YFPT	DSBGA	YFP	28	250	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1

www.ti.com 17-Jun-2015

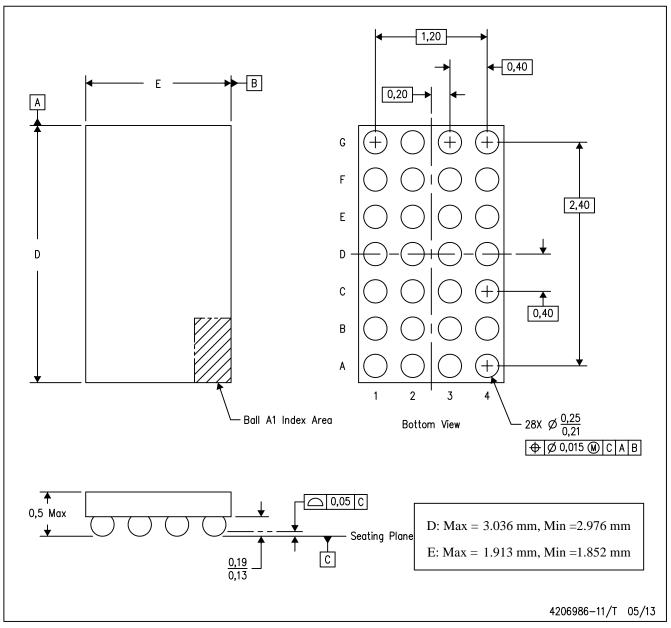


#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
BQ51003YFPR	DSBGA	YFP	28	3000	182.0	182.0	20.0
BQ51003YFPT	DSBGA	YFP	28	250	182.0	182.0	20.0

YFP (R-XBGA-N28)

DIE-SIZE BALL GRID ARRAY



NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. NanoFree™ package configuration.

NanoFree is a trademark of Texas Instruments



#### IMPORTANT NOTICE

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, enhancements, improvements and other changes to its semiconductor products and services per JESD46, latest issue, and to discontinue any product or service per JESD48, latest issue. Buyers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All semiconductor products (also referred to herein as "components") are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its components to the specifications applicable at the time of sale, in accordance with the warranty in TI's terms and conditions of sale of semiconductor products. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by applicable law, testing of all parameters of each component is not necessarily performed.

TI assumes no liability for applications assistance or the design of Buyers' products. Buyers are responsible for their products and applications using TI components. To minimize the risks associated with Buyers' products and applications, Buyers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI components or services are used. Information published by TI regarding third-party products or services does not constitute a license to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of significant portions of TI information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. TI is not responsible or liable for such altered documentation. Information of third parties may be subject to additional restrictions.

Resale of TI components or services with statements different from or beyond the parameters stated by TI for that component or service voids all express and any implied warranties for the associated TI component or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Buyer acknowledges and agrees that it is solely responsible for compliance with all legal, regulatory and safety-related requirements concerning its products, and any use of TI components in its applications, notwithstanding any applications-related information or support that may be provided by TI. Buyer represents and agrees that it has all the necessary expertise to create and implement safeguards which anticipate dangerous consequences of failures, monitor failures and their consequences, lessen the likelihood of failures that might cause harm and take appropriate remedial actions. Buyer will fully indemnify TI and its representatives against any damages arising out of the use of any TI components in safety-critical applications.

In some cases, TI components may be promoted specifically to facilitate safety-related applications. With such components, TI's goal is to help enable customers to design and create their own end-product solutions that meet applicable functional safety standards and requirements. Nonetheless, such components are subject to these terms.

No TI components are authorized for use in FDA Class III (or similar life-critical medical equipment) unless authorized officers of the parties have executed a special agreement specifically governing such use.

Only those TI components which TI has specifically designated as military grade or "enhanced plastic" are designed and intended for use in military/aerospace applications or environments. Buyer acknowledges and agrees that any military or aerospace use of TI components which have not been so designated is solely at the Buyer's risk, and that Buyer is solely responsible for compliance with all legal and regulatory requirements in connection with such use.

TI has specifically designated certain components as meeting ISO/TS16949 requirements, mainly for automotive use. In any case of use of non-designated products, TI will not be responsible for any failure to meet ISO/TS16949.

#### **Products Applications**

logic.ti.com

Audio www.ti.com/audio Automotive and Transportation www.ti.com/automotive **Amplifiers** amplifier.ti.com Communications and Telecom www.ti.com/communications **Data Converters** dataconverter.ti.com Computers and Peripherals www.ti.com/computers **DLP® Products** www.dlp.com Consumer Electronics www.ti.com/consumer-apps DSP dsp.ti.com **Energy and Lighting** www.ti.com/energy Clocks and Timers www.ti.com/clocks Industrial www.ti.com/industrial Interface interface.ti.com Medical www.ti.com/medical Logic Security www.ti.com/security

Power Mgmt Space, Avionics and Defense www.ti.com/space-avionics-defense power.ti.com

Microcontrollers www.ti.com/video microcontroller.ti.com Video and Imaging

www.ti-rfid.com

**OMAP Applications Processors TI E2E Community** www.ti.com/omap e2e.ti.com

Wireless Connectivity www.ti.com/wirelessconnectivity