

# TPS564201 4.5-V to 17-V Input, 4-A Synchronous Step-Down Voltage Regulator in SOT-23

## 1 Features

- TPS564201 4-A Converter Integrated 50-mΩ and 22-mΩ FETs
- D-CAP2™ Mode Control with Fast Transient Response
- Input Voltage Range: 4.5 V to 17 V
- Output Voltage Range: 0.76 V to 7 V
- Pulse Skip Mode
- 560-kHz Switching Frequency
- Low Shutdown Current Less than 5 μA
- 2.5% Feedback Voltage Accuracy (25°C)
- Startup from Pre-Biased Output Voltage
- Cycle-by-Cycle Overcurrent Limit
- Hiccup-mode Overcurrent Protection
- Non-Latch UVP and TSD Protections
- Fixed Soft Start: 1.0 ms

## 2 Applications

- Digital TV Power Supply
- High Definition Blu-ray™ Disc Players
- Networking Home Terminal
- Digital Set Top Box (STB)
- Surveillance

## 3 Description

The TPS564201 is a simple, easy-to-use, 4-A synchronous step-down converter in SOT-23 package.

The device is optimized to operate with minimum external component count and also optimized to achieve low standby current.

These switch mode power supply (SMPS) devices employ D-CAP2 mode control providing a fast transient response and supporting both low-equivalent series resistance (ESR) output capacitors such as specialty polymer and ultra-low ESR ceramic capacitors with no external compensation components.

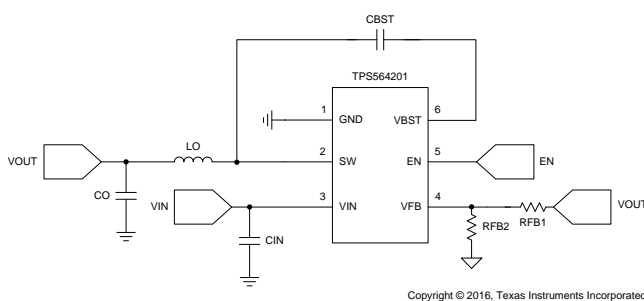
The TPS564201 operates in pulse skip mode, maintaining high efficiency during light load operation. The TPS564201 is available in a 6-pin 1.6-mm × 2.9-mm SOT (DDC) package, and specified from a –40°C to 125°C junction temperature.

### Device Information<sup>(1)</sup>

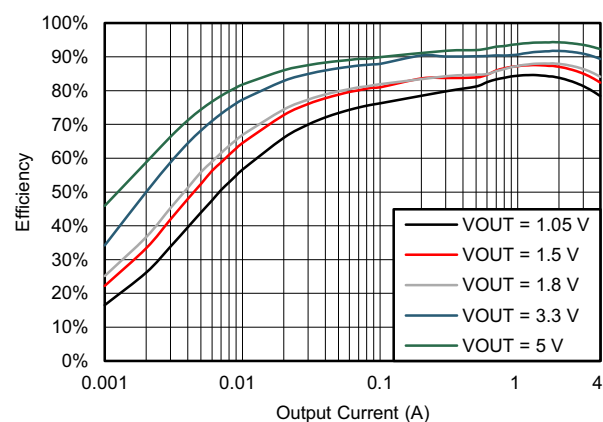
PART NUMBER	PACKAGE	BODY SIZE (NOM)
TPS564201	DDC (6)	1.60 mm × 2.90 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

### Simplified Schematic



### TPS564201 Efficiency



## Table of Contents

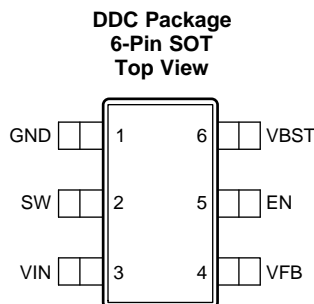
<b>1 Features</b> .....	<b>1</b>	7.3 Feature Description.....	<b>9</b>
<b>2 Applications</b> .....	<b>1</b>	7.4 Device Functional Modes.....	<b>11</b>
<b>3 Description</b> .....	<b>1</b>	<b>8 Application and Implementation</b> .....	<b>12</b>
<b>4 Revision History</b> .....	<b>2</b>	8.1 Application Information.....	<b>12</b>
<b>5 Pin Configuration and Functions</b> .....	<b>3</b>	8.2 Typical Application .....	<b>12</b>
<b>6 Specifications</b> .....	<b>3</b>	<b>9 Power Supply Recommendations</b> .....	<b>17</b>
6.1 Absolute Maximum Ratings .....	<b>3</b>	<b>10 Layout</b> .....	<b>18</b>
6.2 ESD Ratings.....	<b>3</b>	10.1 Layout Guidelines .....	<b>18</b>
6.3 Recommended Operating Conditions.....	<b>4</b>	10.2 Layout Example .....	<b>18</b>
6.4 Thermal Information .....	<b>4</b>	<b>11 Device and Documentation Support</b> .....	<b>19</b>
6.5 Electrical Characteristics.....	<b>5</b>	11.1 Community Resources.....	<b>19</b>
6.6 Typical Characteristics.....	<b>6</b>	11.2 Trademarks .....	<b>19</b>
<b>7 Detailed Description</b> .....	<b>9</b>	11.3 Electrostatic Discharge Caution.....	<b>19</b>
7.1 Overview .....	<b>9</b>	11.4 Glossary .....	<b>19</b>
7.2 Functional Block Diagram .....	<b>9</b>	<b>12 Mechanical, Packaging, and Orderable Information</b> .....	<b>19</b>

## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Original (May 2016) to Revision A</b>	<b>Page</b>
• Full specification release .....	<b>1</b>

## 5 Pin Configuration and Functions



### Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
GND	1	—	Ground pin Source terminal of low-side power NFET as well as the ground terminal for controller circuit. Connect sensitive VFB to this GND at a single point.
SW	2	O	Switch node connection between high-side NFET and low-side NFET.
VIN	3	I	Input voltage supply pin. The drain terminal of high-side power NFET.
VFB	4	I	Converter feedback input. Connect to output voltage with feedback resistor divider.
EN	5	I	Enable input control. Active high and must be pulled up to enable the device.
VBST	6	O	Supply input for the high-side NFET gate drive circuit. Connect 0.1 $\mu$ F capacitor between VBST and SW pins.

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Input voltage	VIN, EN	−0.3	19	V
	VBST	−0.3	25	V
	VBST (10 ns transient)	−0.3	27	V
	VBST (vs SW)	−0.3	6.5	V
	VFB	−0.3	6.5	V
	SW	−2	19	V
	SW (10 ns transient)	−3.5	21	V
Operating junction temperature, T <sub>J</sub>		−40	150	°C
Storage temperature, T <sub>stg</sub>		−55	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 6.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub> Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±4000	V
	Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.  
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
$V_{IN}$	Supply input voltage range	4.5		17	V
$V_I$	Input voltage range	VBST		23	V
		VBST (10 ns transient)	-0.1	26	
		VBST (vs SW)	-0.1	6.0	
		EN	-0.1	17	
		VFB	-0.1	5.5	
		SW	-1.8	17	
		SW (10 ns transient)	-3.5	20	
$T_J$	Operating junction temperature	-40		125	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TPS564201	UNIT
		DDC (SOT)	
		6 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	86.3	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	39.4	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	13.3	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	1.8	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	13.3	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

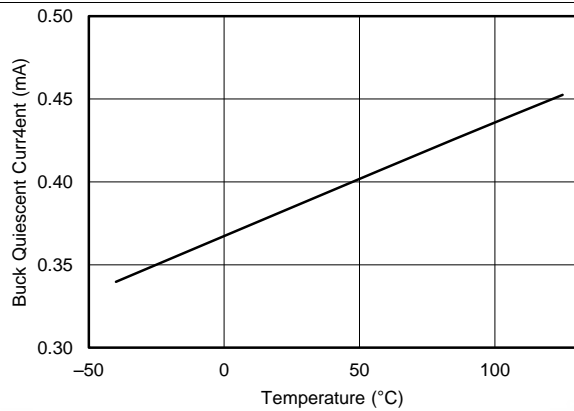
## 6.5 Electrical Characteristics

 $T_J = -40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ ,  $V_{IN} = 12\text{ V}$  (unless otherwise noted)

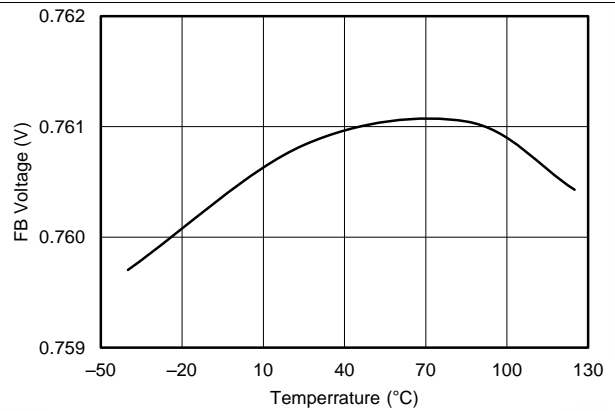
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>SUPPLY CURRENT</b>						
$I_{VIN}$	Operating – non-switching supply current	$V_{IN}$ current, $EN = 5\text{ V}$ , $V_{FB} = 1\text{ V}$		400	510	$\mu\text{A}$
$I_{VINS DN}$	Shutdown supply current	$V_{IN}$ current, $EN = 0\text{ V}$		0.9	5	$\mu\text{A}$
<b>LOGIC THRESHOLD</b>						
$V_{ENH}$	EN high-level input voltage	EN	1.6			V
$V_{ENL}$	EN low-level input voltage	EN			0.8	V
$R_{EN}$	EN pin resistance to GND	$V_{EN} = 12\text{ V}$	225	425	900	$\text{k}\Omega$
<b><math>V_{FB}</math> VOLTAGE AND DISCHARGE RESISTANCE</b>						
$V_{FBTH}$	$V_{FB}$ threshold voltage	$V_O = 1.05\text{ V}$ , continuous mode operation	739	759	779	mV
$I_{VFB}$	$V_{FB}$ input current	$V_{FB} = 0.8\text{ V}$		0	$\pm 0.1$	$\mu\text{A}$
<b>MOSFET</b>						
$R_{DS(on)h}$	High-side switch resistance	$T_A = 25^{\circ}\text{C}$ , $V_{BST} - SW = 5.5\text{ V}$		50		$\text{m}\Omega$
$R_{DS(on)l}$	Low-side switch resistance	$T_A = 25^{\circ}\text{C}$		22		$\text{m}\Omega$
<b>CURRENT LIMIT</b>						
$I_{ocL}$	Current limit <sup>(1)</sup>	DC current, $V_{OUT} = 1.05\text{ V}$ , $L_1 = 1.5\text{ }\mu\text{H}$	4.2	6	7.7	A
<b>THERMAL SHUTDOWN</b>						
$T_{SDN}$	Thermal shutdown threshold <sup>(1)</sup>	Shutdown temperature		172		$^{\circ}\text{C}$
		Hysteresis		38		
<b>ON-TIME TIMER CONTROL</b>						
$t_{OFF(MIN)}$	Minimum off time	$V_{FB} = 0.68\text{ V}$		220	280	ns
<b>SOFT START</b>						
$t_{SS}$	Soft-start time	Internal soft-start time		1.0		ms
<b>FREQUENCY</b>						
$F_{sw}$	Switching frequency	$V_{IN} = 12\text{ V}$ , $V_O = 1.05\text{ V}$ , FCCM mode		560		kHz
<b>OUTPUT UNDERVOLTAGE AND OVERVOLTAGE PROTECTION</b>						
$V_{UVP}$	Output UVP threshold	Hiccup detect ( $H > L$ )		65%		
$T_{HICCUP\_WAIT}$	Hiccup on time			1.9		ms
$T_{HICCUP\_RE}$	Hiccup time before restart			15.5		ms
<b>UVLO</b>						
UVLO	UVLO threshold	Wake up VIN voltage		4.0	4.3	V
		Shutdown VIN voltage	3.3	3.6		
		Hysteresis VIN voltage <sup>(1)</sup>		0.4		

(1) Not production tested.

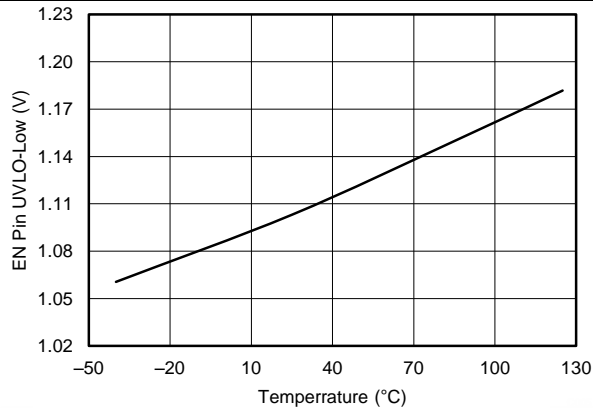
## 6.6 Typical Characteristics

 $V_{IN} = 12\text{ V}$  (unless otherwise noted)


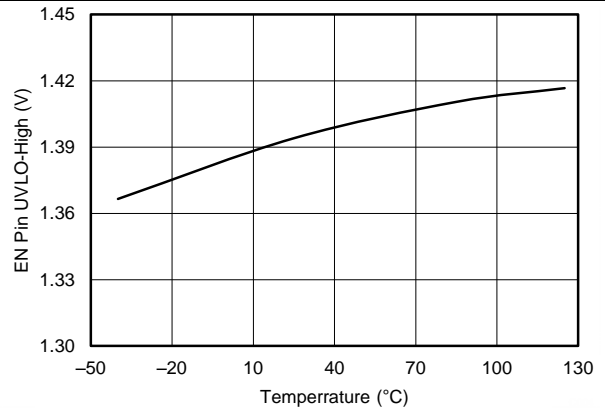
**Figure 1. TPS564201 Supply Current vs Junction Temperature**



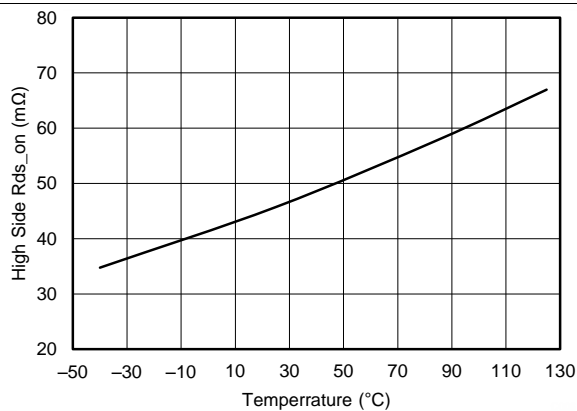
**Figure 2. VFB Voltage vs Junction Temperature**



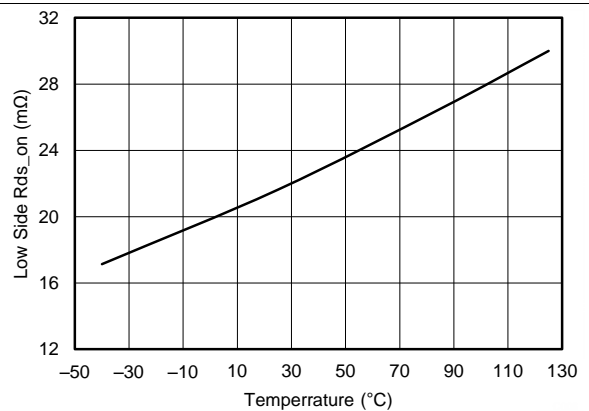
**Figure 3. EN Pin UVLO Low Voltage vs Junction Temperature**



**Figure 4. TPS564201 EN Pin UVLO High Voltage vs Junction Temperature**



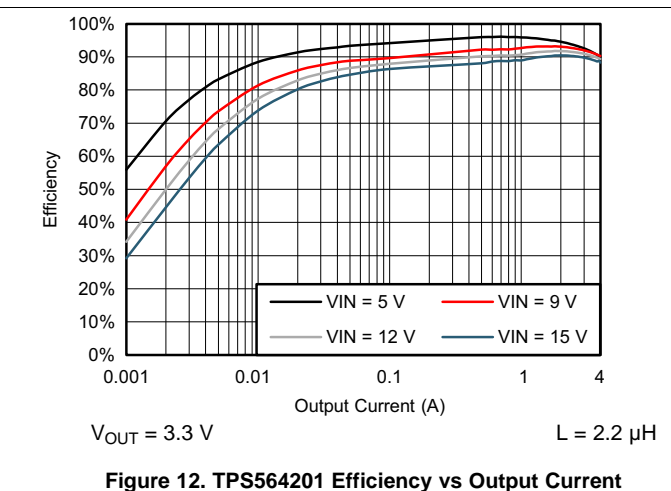
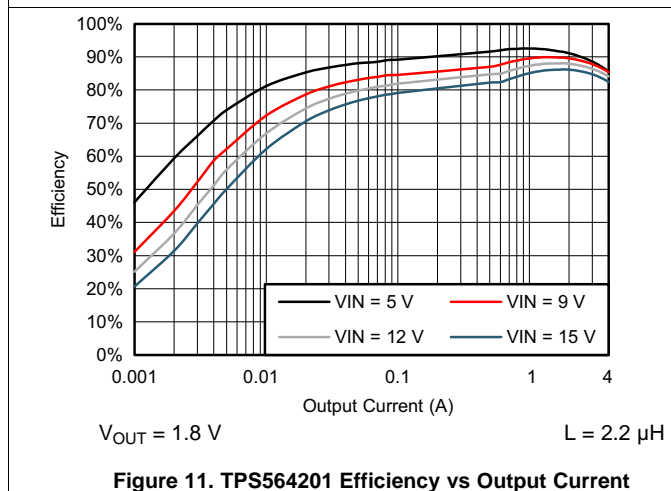
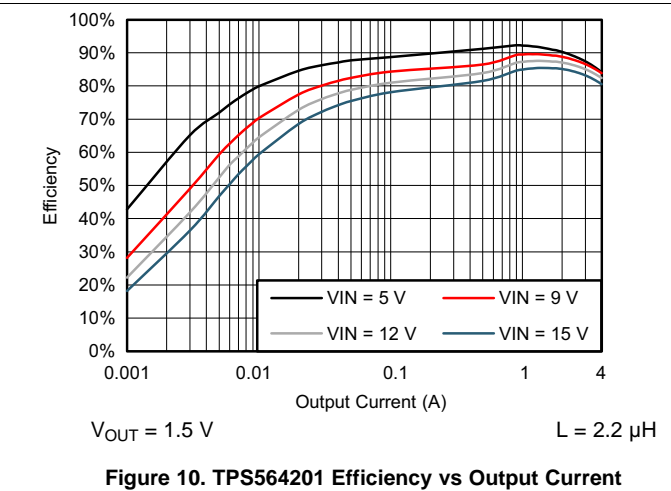
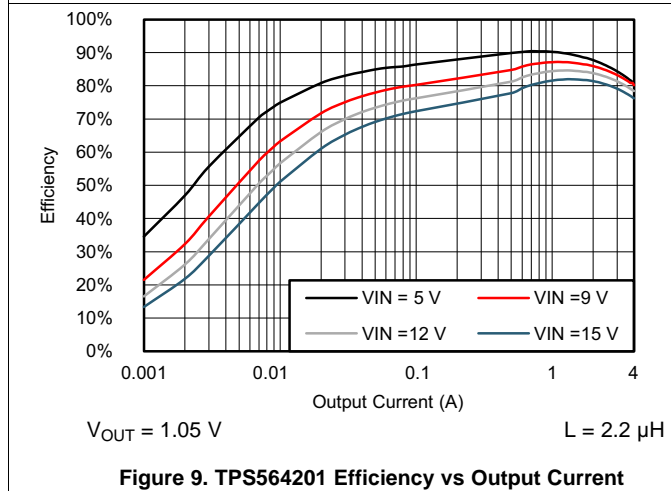
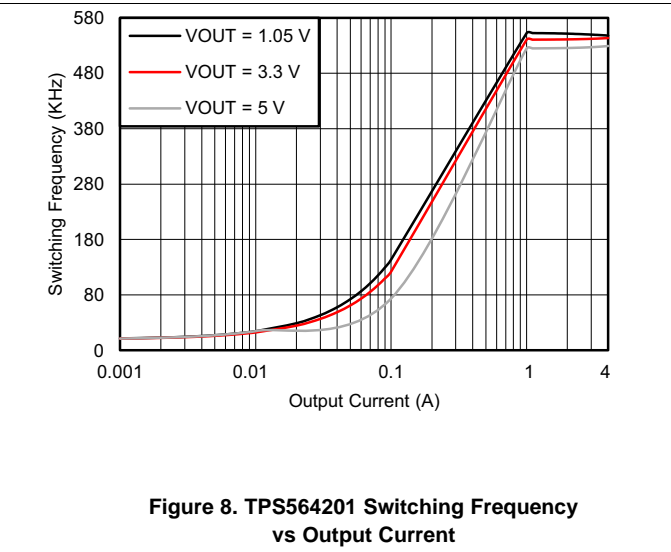
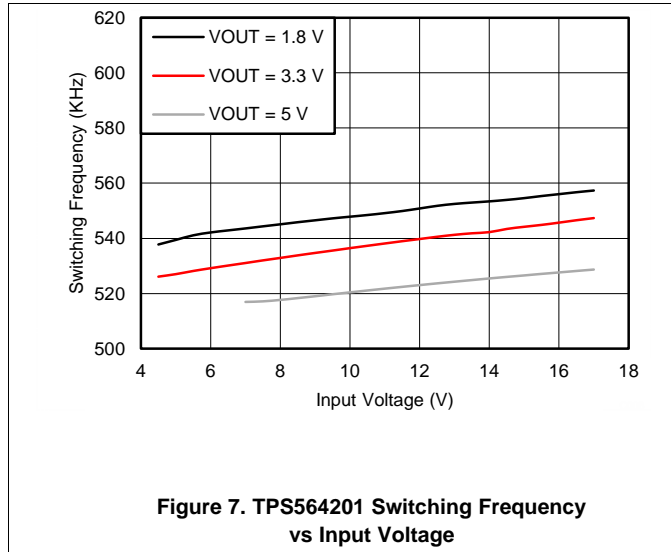
**Figure 5. TPS564201 High-Side  $R_{ds-On}$  vs Junction Temperature**



**Figure 6. Low-Side  $R_{ds-On}$  vs Junction Temperature**

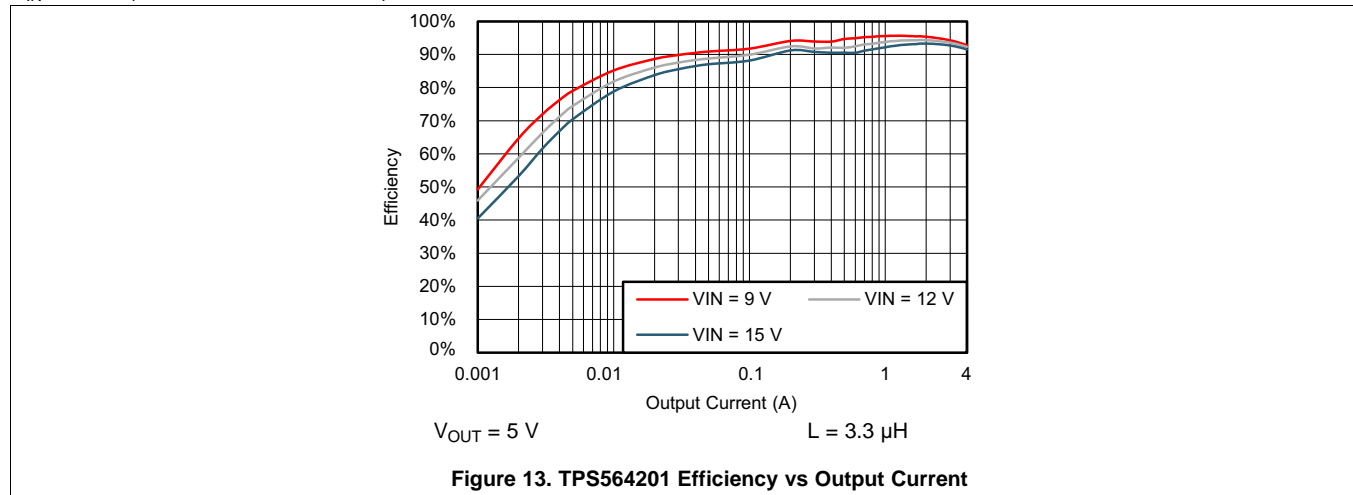
Typical Characteristics (continued)

V<sub>IN</sub> = 12 V (unless otherwise noted)



Typical Characteristics (continued)

$V_{IN} = 12\text{ V}$  (unless otherwise noted)



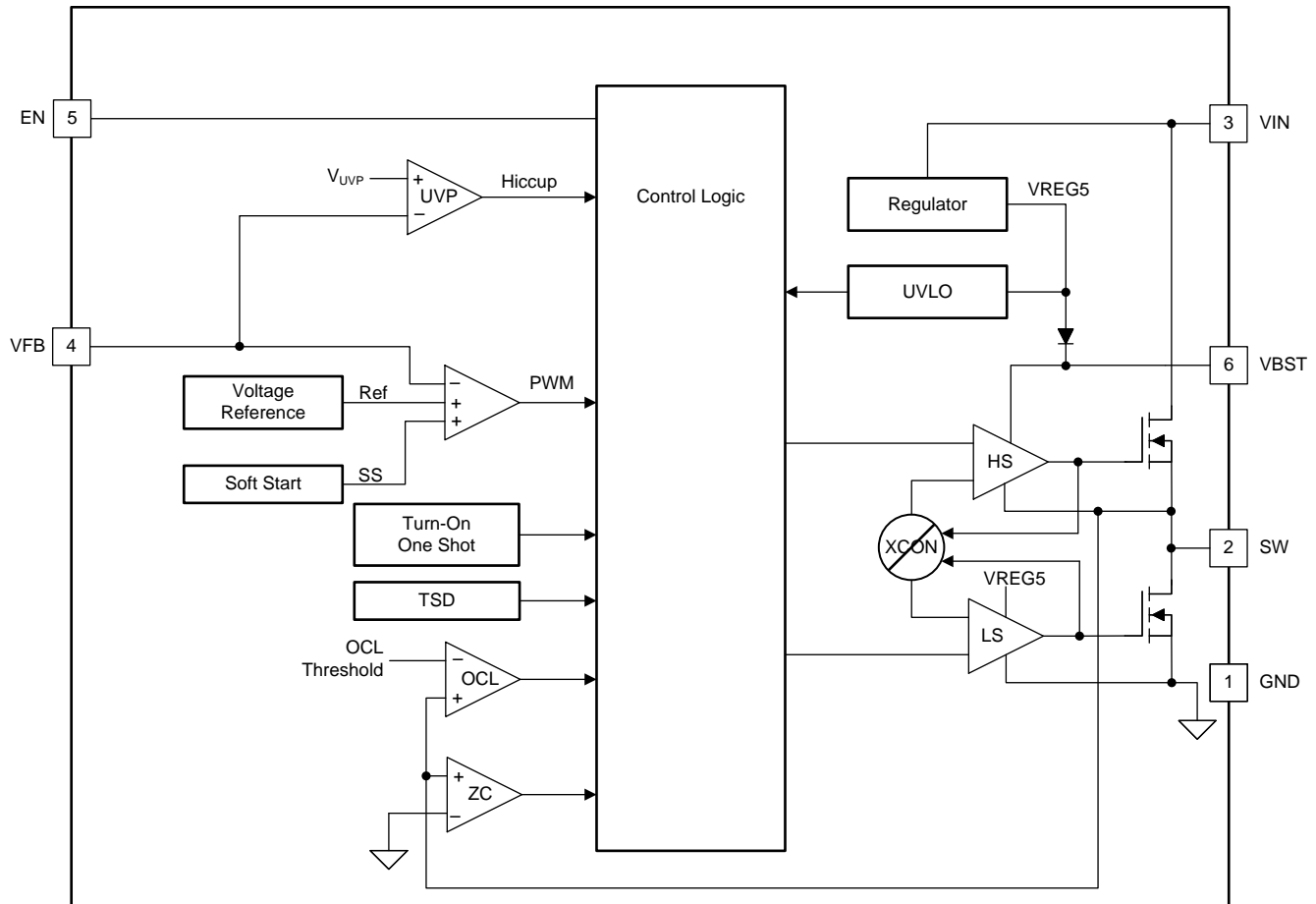


## 7 Detailed Description

### 7.1 Overview

The TPS564201 is a 4-A synchronous step-down converter. The proprietary D-CAP2™ mode control supports low ESR output capacitors such as specialty polymer capacitors and multi-layer ceramic capacitors without complex external compensation circuits. The fast transient response of D-CAP2™ mode control can reduce the output capacitance required to meet a specific level of performance.

### 7.2 Functional Block Diagram



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### 7.3 Feature Description

#### 7.3.1 Adaptive On-Time Control and PWM Operation

The main control loop of the TPS564201 is adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2™ mode control. The D-CAP2™ mode control combines adaptive on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low-ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

## Feature Description (continued)

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off after internal one-shot timer expires. This one shot duration is set inversely proportional to the converter input voltage,  $V_{IN}$ , and proportional to the output voltage  $V_O$ , to maintain a pseudo-fixed frequency over the input voltage range, hence it is called adaptive on-time control. The one-shot timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the reference voltage. An internal ramp is added to reference voltage to simulate output ripple, eliminating the need for ESR induced output ripple from D-CAP2™ mode control.

### 7.3.2 Pulse Skip Mode

The TPS564201 is designed with Advanced Eco-mode™ to maintain high light load efficiency. As the output current decreases from heavy load condition, the inductor current is also reduced and eventually comes to point that its rippled valley touches zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when the zero inductor current is detected. As the load current further decreases the converter runs into discontinuous conduction mode. The on-time is kept almost the same as it was in the continuous conduction mode so that it takes longer time to discharge the output capacitor with smaller load current to the level of the reference voltage. This makes the switching frequency lower, proportional to the load current, and keeps the light load efficiency high. The transition point to the light load operation IOUT(LL) current can be calculated in [Equation 1](#).

$$I_{OUT(LL)} = \frac{1}{2 \times L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}} \quad (1)$$

### 7.3.3 Soft Start and Pre-Biased Soft Start

The TPS564201 has an internal 1.0-ms soft-start. When the EN pin becomes high, the internal soft-start function begins ramping up the reference voltage to the PWM comparator.

If the output capacitor is pre-biased at startup, the device initiates switching and starts ramping up only after the internal reference voltage becomes greater than the feedback voltage  $V_{FB}$ . This scheme ensures that the converter ramps up smoothly into regulation point.

### 7.3.4 Current Protection

The output over-current limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. To improve accuracy, the voltage sensing is temperature compensated.

During the on time of the high-side FET switch, the switch current increases at a linear rate determined by  $V_{IN}$ ,  $V_{OUT}$ , the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current  $I_{out}$ . If the monitored current is above the OCL level, the converter maintains low-side FET on and delays the creation of a new set pulse, even the voltage feedback loop requires one, until the current level becomes OCL level or lower. In subsequent switching cycles, the on-time is set to a fixed value and the current is monitored in the same manner.

There are some important considerations for this type of over-current protection. The load current is higher than the over-current threshold by one half of the peak-to-peak inductor ripple current. Also, when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. This may cause the output voltage to fall. When the  $V_{FB}$  voltage falls below the UVP threshold voltage, the UVP comparator detects it. And then, the device shuts down after the UVP delay time (typically 24  $\mu$ s) and re-starts after the hiccup time (typically 15.5 ms).

When the over current condition is removed, the output voltage returns to the regulated value.

### 7.3.5 Undervoltage Lockout (UVLO) Protection

UVLO protection monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

## Feature Description (continued)

### 7.3.6 Thermal Shutdown

The device monitors the temperature of itself. If the temperature exceeds the threshold value (typically 172°C), the device is shut off. This is a non-latch protection.

## 7.4 Device Functional Modes

### 7.4.1 Normal Operation

When the input voltage is above the UVLO threshold and the EN voltage is above the enable threshold, the TPS564201 operates in the normal switching mode. Normal continuous conduction mode (CCM) occurs when the minimum switch current is above 0 A. In CCM, the TPS564201 operates at a quasi-fixed frequency of 560 kHz.

### 7.4.2 Eco-mode™ Operation

When the TPS564201 is in the normal CCM operating mode and the switch current falls to 0A, the TPS564201 begins operating in pulse skipping eco-mode. Each switching cycle is followed by a period of energy saving sleep time. The sleep time ends when the VFB voltage falls below the eco-mode threshold voltage. As the output current decreases, the perceived time between switching pulses increases.

### 7.4.3 Standby Operation

When the TPS564201 is operating in either normal CCM or Eco-mode™, it may be placed in standby by asserting the EN pin low.

## 8 Application and Implementation

### NOTE

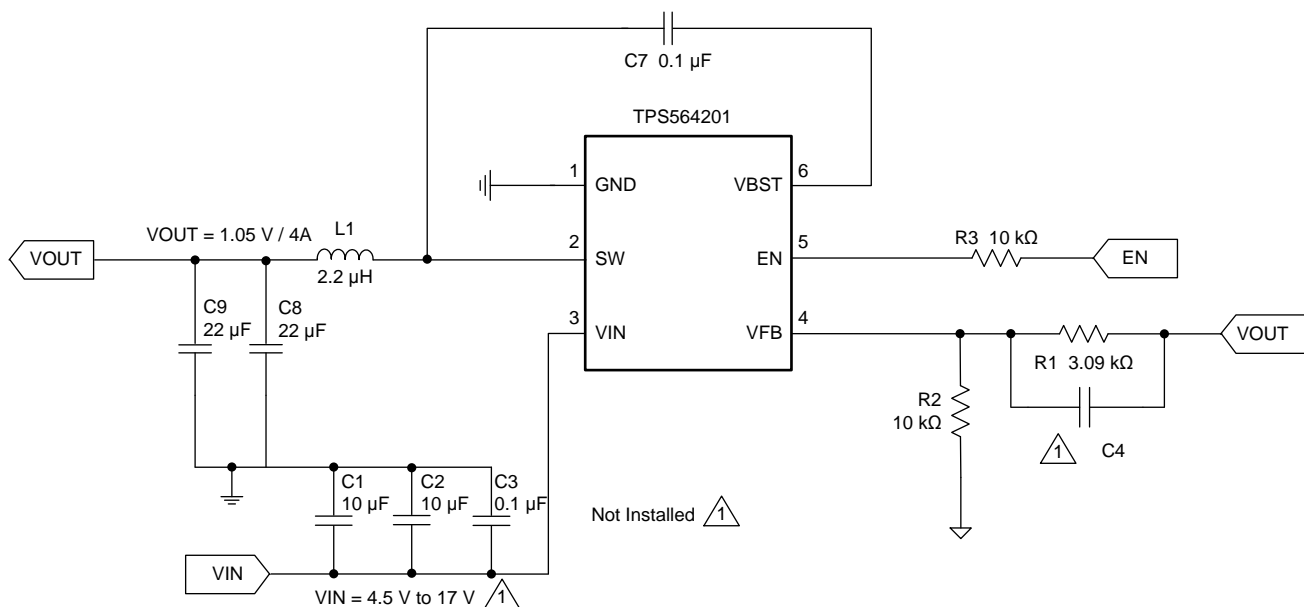
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The device is a typical step-down DC-DC converter for converting a higher dc voltage to a lower dc voltage with a maximum available output current of 4 A. The following design procedure can be used to select component values for the TPS564201. Alternately, the WEBENCH® software may be used to generate a complete design. The WEBENCH software uses an iterative design procedure and accesses a comprehensive database of components when generating a design. This section presents a simplified discussion of the design process.

### 8.2 Typical Application

The application schematic in Figure 14 shows the TPS564201 4.5-V to 17-V input, 1.05-V output converter design meeting the requirements for 4-A output. This circuit is available as the evaluation module (EVM). The sections provide the design procedure.



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Figure 14. TPS564201 1.05-V, 4-A Reference Design

## Typical Application (continued)

### 8.2.1 Design Requirements

Table 1 shows the design parameters for this application.

**Table 1. Design Parameters**

PARAMETER	EXAMPLE VALUE
Input voltage range	4.5 to 17 V
Output voltage	1.05 V
Transient response, 2-A load step	$\Delta V_{out} = \pm 5\%$
Input ripple voltage	400 mV
Output ripple voltage	30 mV
Output current rating	4 A
Operating frequency	560 kHz

### 8.2.2 Detailed Design Procedure

#### 8.2.2.1 Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the VFB pin. TI recommends to use 1% tolerance or better divider resistors. Start by using Equation 2 to calculate  $V_{OUT}$ .

To improve efficiency at very light loads consider using larger value resistors. However, using too high of resistance causes the circuit to be more susceptible to noise; and, voltage errors from the VFB input current will be more noticeable.

$$V_{OUT} = 0.759 \times \left( 1 + \frac{R1}{R2} \right) \quad (2)$$

#### 8.2.2.2 Output Filter Selection

The LC filter used as the output filter has double pole at:

$$f_p = \frac{1}{2\pi\sqrt{L_{OUT} \times C_{OUT}}} \quad (3)$$

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the device. The low frequency phase is 180°. At the output filter pole frequency, the gain rolls off at a –40 dB per decade rate and the phase drops rapidly. D-CAP2 introduces a high frequency zero that reduces the gain roll off to –20 dB per decade and increases the phase to 90° one decade above the zero frequency. The inductor and capacitor for the output filter must be selected so that the double pole of Equation 3 is located below the high frequency zero but close enough that the phase boost provided by the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in Table 2.

**Table 2. Recommended Component Values**

OUTPUT VOLTAGE (V)	R1 (kΩ)	R2 (kΩ)	L1 (μH)			C8 + C9 (μF)
			MIN	TYP	MAX	
1	3.09	10.0	1.5	2.2	4.7	20 to 68
1.05	3.74	10.0	1.5	2.2	4.7	20 to 68
1.2	5.76	10.0	1.5	2.2	4.7	20 to 68
1.5	9.53	10.0	1.5	2.2	4.7	20 to 68
1.8	13.7	10.0	1.5	2.2	4.7	20 to 68
2.5	22.6	10.0	2.2	2.2	4.7	20 to 68
3.3	33.2	10.0	2.2	2.2	4.7	20 to 68
5	54.9	10.0	3.3	3.3	4.7	20 to 68
6.5	75	10.0	3.3	3.3	4.7	20 to 68

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 4](#), [Equation 5](#), and [Equation 6](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current.

Use 560 kHz for  $f_{SW}$ . Make sure the chosen inductor is rated for the peak current of [Equation 5](#) and the RMS current of [Equation 7](#).

$$I_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (4)$$

$$I_{PEAK} = I_O + \frac{I_{P-P}}{2} \quad (5)$$

$$I_{LO(RMS)} = \sqrt{I_O^2 + \frac{1}{12} I_{P-P}^2} \quad (6)$$

For this design example, the calculated peak current is 4.4 A and the calculated RMS current is 4 A. The inductor used is a WE 74431122 with a peak current rating of 13 A and an RMS current rating of 9 A.

The capacitor value and ESR determines the amount of output voltage ripple. The TPS564201 is intended for use with ceramic or other low ESR capacitors. Recommended values range from 20  $\mu$ F to 68  $\mu$ F. Use [Equation 7](#) to determine the required RMS current rating for the output capacitor.

$$I_{CO(RMS)} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{\sqrt{12} \times V_{IN} \times L_O \times f_{SW}} \quad (7)$$

For this design two TDK C3216X5R0J226M 22- $\mu$ F output capacitors are used. The typical ESR is 2 m $\Omega$  each. The calculated RMS current is 0.286 A and each output capacitor is rated for 4 A.

### 8.2.2.3 Input Capacitor Selection

The TPS564201 requires an input decoupling capacitor and a bulk capacitor is needed depending on the application. TI recommends a ceramic capacitor over 10  $\mu$ F for the decoupling capacitor. An additional 0.1- $\mu$ F capacitor (C3) from pin 3 to ground is optional to provide additional high frequency filtering. The capacitor voltage rating needs to be greater than the maximum input voltage.

### 8.2.2.4 Bootstrap Capacitor Selection

A 0.1- $\mu$ F ceramic capacitor must be connected between the VBST to SW pin for proper operation. TI recommends to use a ceramic capacitor.

### 8.2.3 Application Curves

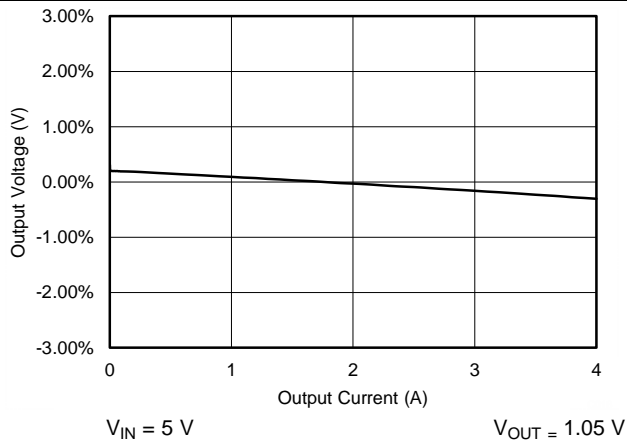


Figure 15. Load Regulation,  $V_{IN} = 5\text{ V}$

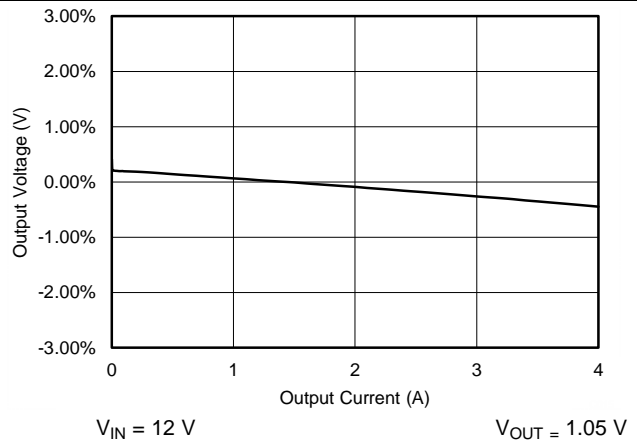


Figure 16. Load Regulation,  $V_{IN} = 12\text{ V}$

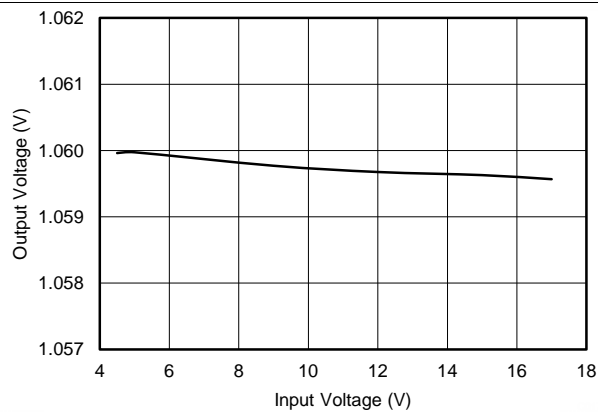


Figure 17. Line Regulation

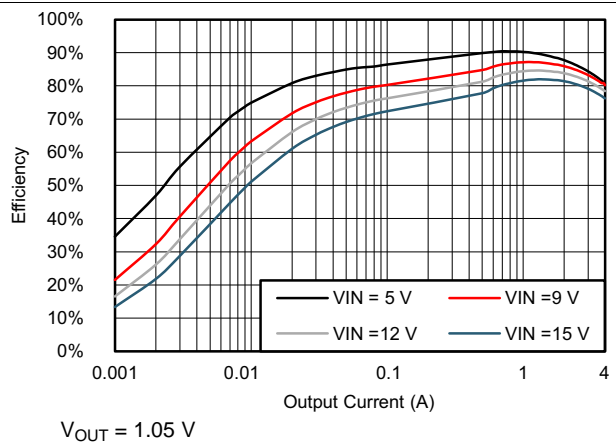


Figure 18. Efficiency vs Output Current

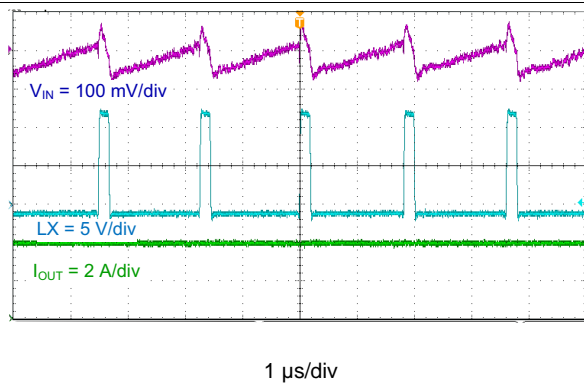


Figure 19. TPS564201 Input Voltage Ripple

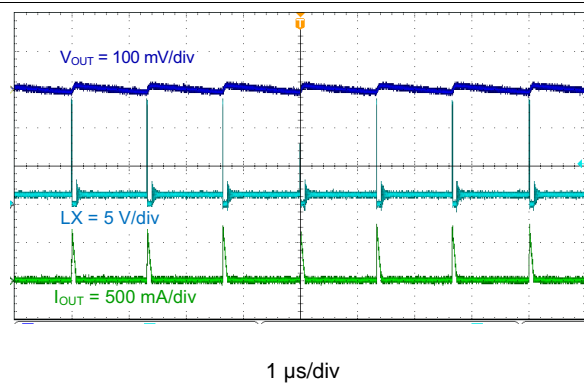
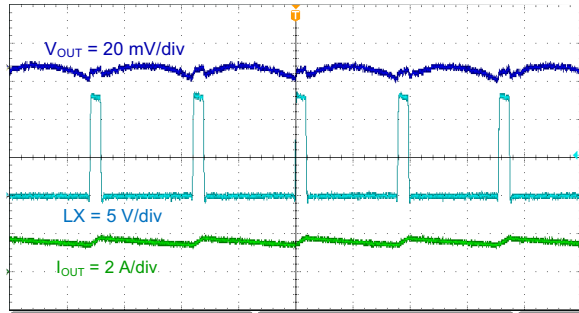
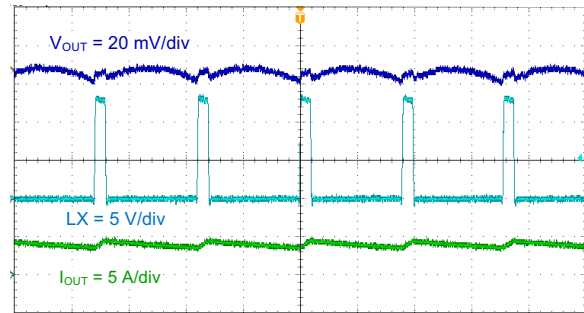


Figure 20. TPS564201 Output Voltage Ripple, No Load



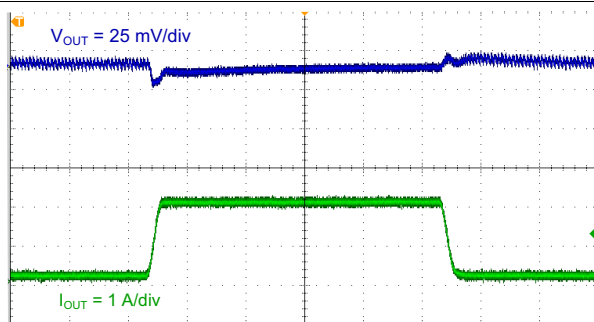
1  $\mu$ s/div

Figure 21. TPS564201 Output Voltage Ripple,  $I_{OUT}$  2 A



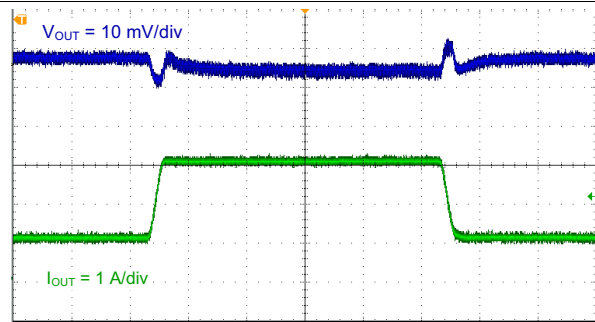
1  $\mu$ s/div

Figure 22. TPS564201 Output Voltage Ripple,  $I_{OUT}$  4 A



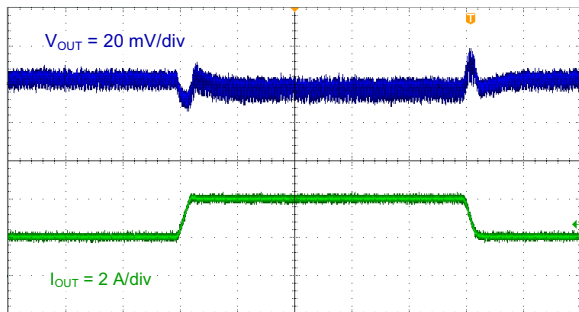
100  $\mu$ s/div

Figure 23. TPS564201 Transient Response 0.1 to 2 A



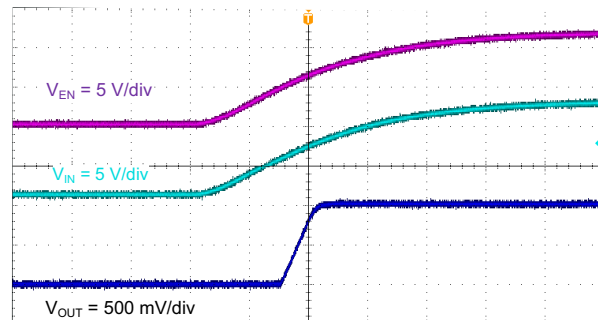
100  $\mu$ s/div

Figure 24. TPS564201 Transient Response, 1 to 3 A



100  $\mu$ s/div

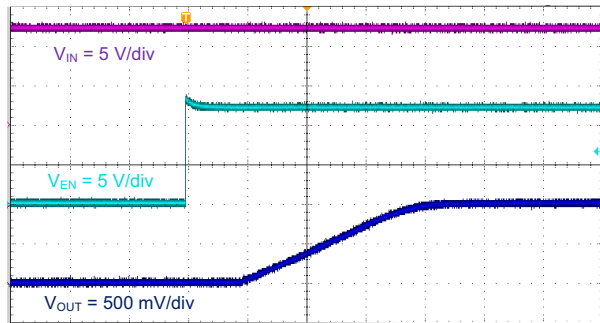
Figure 25. TPS564201 Transient Response, 2 to 4 A



2 ms/div

Figure 26. TPS564201 Startup Relative to  $V_{IN}$





400 μs/div

Figure 27. TPS564201 Startup Relative to EN

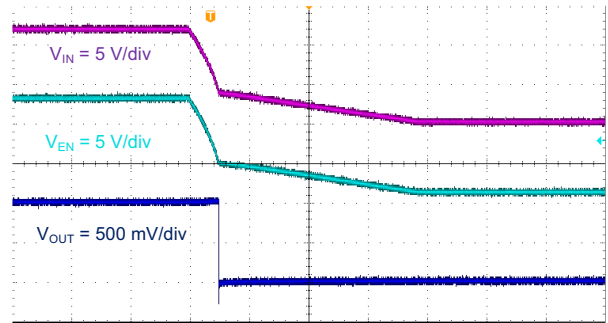


Figure 28. TPS564201 Shutdown Relative to VIN

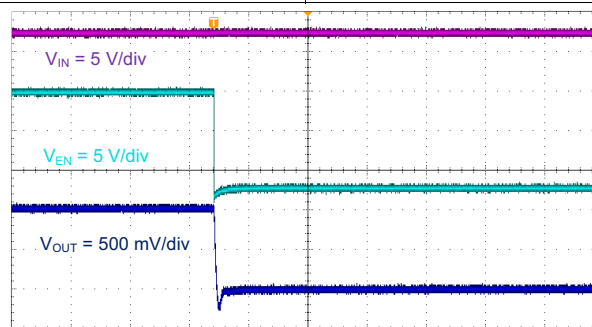


Figure 29. TPS564201 Shutdown Relative to EN

## 9 Power Supply Recommendations

The TPS564201 is designed to operate from input supply voltage in the range of 4.5 V to 17 V. Buck converters require the input voltage to be higher than the output voltage for proper operation. The maximum recommended operating duty cycle is 75%. Using that criteria, the minimum recommended input voltage is  $V_O / 0.75$ .

## 10 Layout

### 10.1 Layout Guidelines

1. VIN and GND traces should be as wide as possible to reduce trace impedance. The wide areas are also of advantage from the view point of heat dissipation.
2. The input capacitor and output capacitor should be placed as close to the device as possible to minimize trace impedance.
3. Provide sufficient vias for the input capacitor and output capacitor.
4. Keep the SW trace as physically short and wide as practical to minimize radiated emissions.
5. Do not allow switching current to flow under the device.
6. A separate VOUT path should be connected to the upper feedback resistor.
7. Make a Kelvin connection to the GND pin for the feedback path.
8. Voltage feedback loop should be placed away from the high-voltage switching trace, and preferably has ground shield.
9. The trace of the VFB node should be as small as possible to avoid noise coupling.
10. The GND trace between the output capacitor and the GND pin should be as wide as possible to minimize its trace impedance.

### 10.2 Layout Example

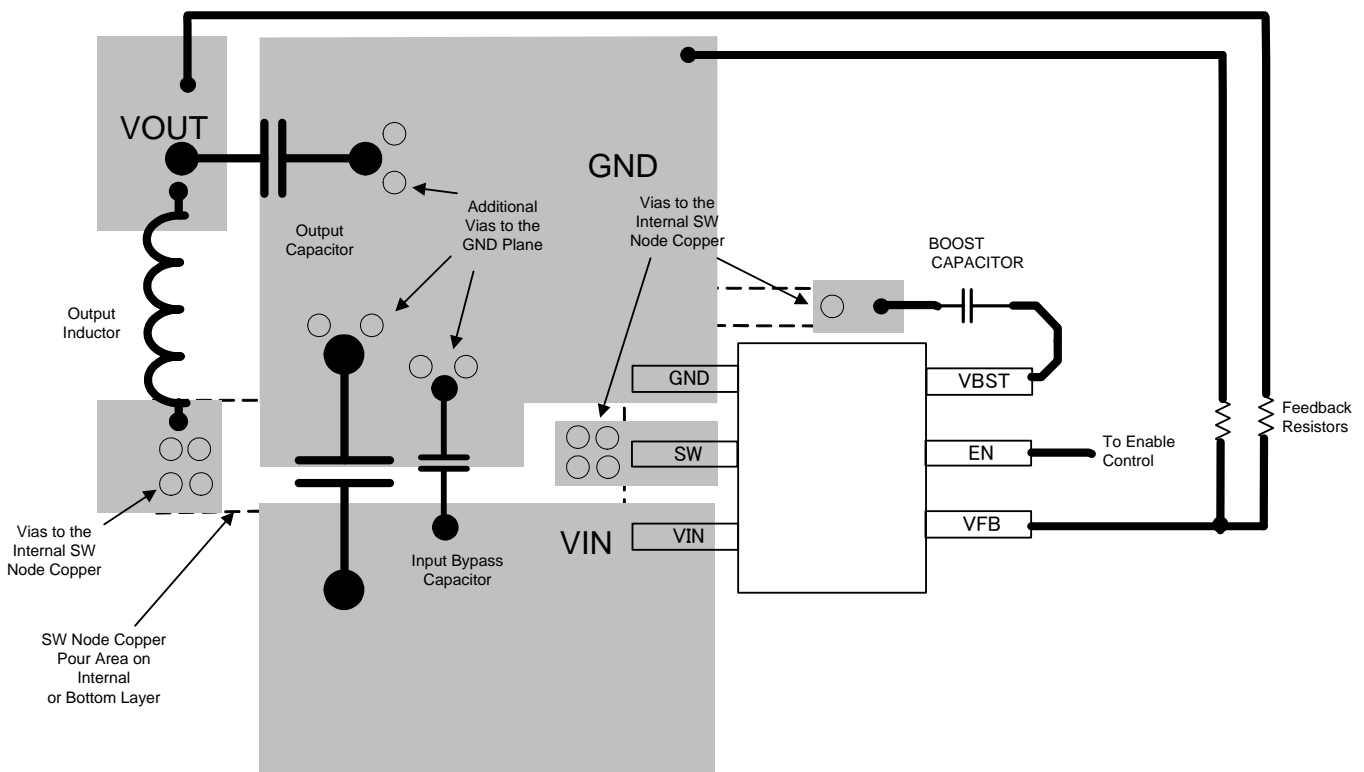


Figure 30. TPS564201 Layout Example

## 11 Device and Documentation Support

### 11.1 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At [e2e.ti.com](http://e2e.ti.com), you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

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### 11.3 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 11.4 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS564201DDCR	ACTIVE	SOT	DDC	6	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	4201	<a href="#">Samples</a>
TPS564201DDCT	ACTIVE	SOT	DDC	6	250	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	4201	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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## TAPE AND REEL INFORMATION



### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS564201DDCR	SOT	DDC	6	3000	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3
TPS564201DDCT	SOT	DDC	6	250	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3

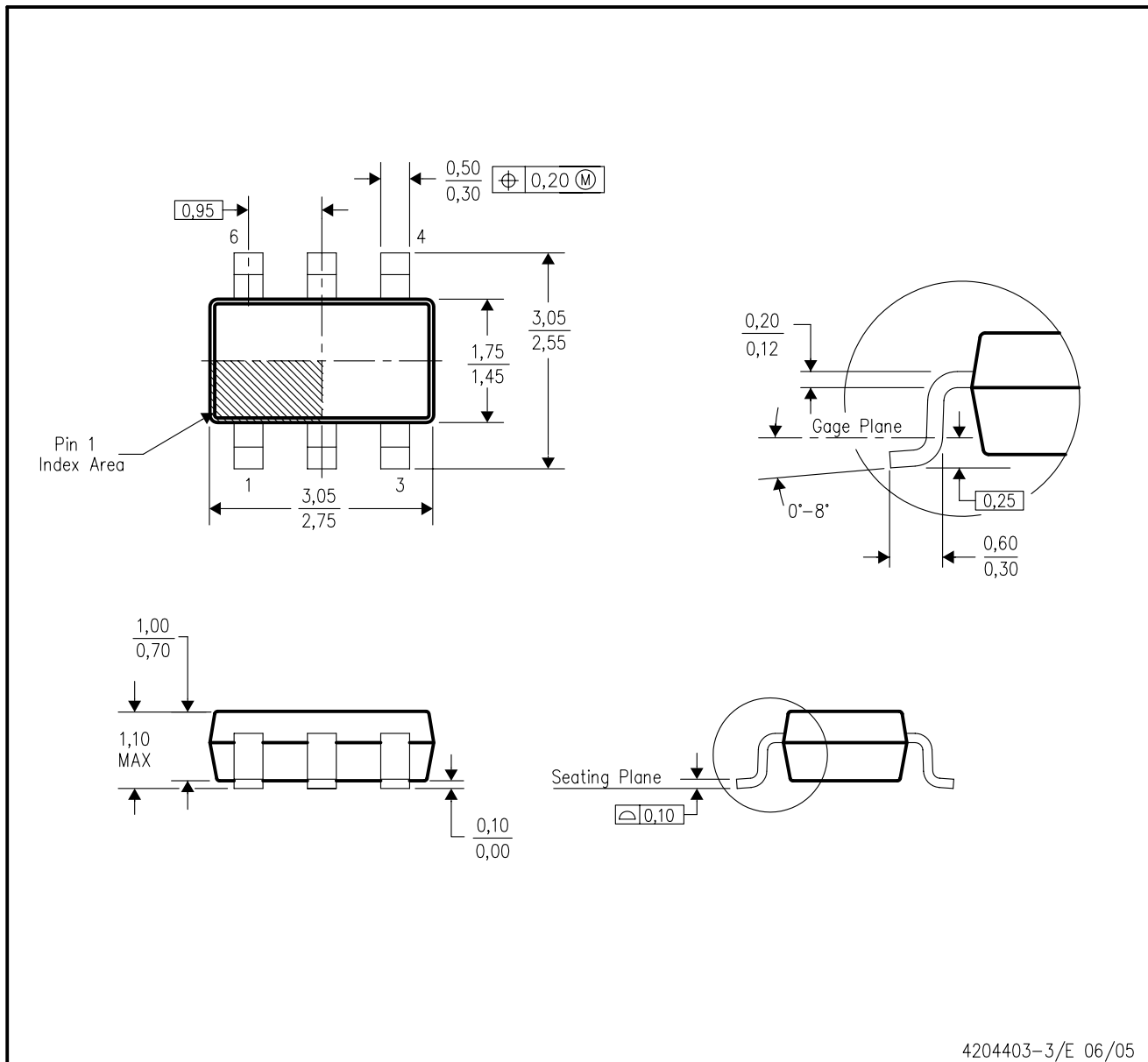
**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS564201DDCR	SOT	DDC	6	3000	184.0	184.0	19.0
TPS564201DDCT	SOT	DDC	6	250	184.0	184.0	19.0

DDC (R-PDSO-G6)

PLASTIC SMALL-OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Body dimensions do not include mold flash or protrusion.
  - Falls within JEDEC MO-193 variation AA (6 pin).



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